ASD-TR-80-5036

METHOD FOR GENERATING A RANDOMIZED FLIGHT-BY-FLIGHT LOADING SEQUENCE FOR AN AIRCRAFT

JOHN W. LINCOLN
STRUCTURES DIVISION
DIRECTORATE OF FLIGHT SYSTEMS ENGINEERING

JULY 1980

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED

DEPUTY FOR ENGINEERING AERONAUTICAL SYSTEMS DIVISION AIR FORCE SYSTEMS COMMAND WRIGHT-PATTERSON AIR FORCE BASE, OH

Copy available to DTIC does not permit fully legible reproduction



82 03 17 124

FILE BOPY

NOTICE

When Government drawings, specifications, or other data are used for any purpose other than in connection with a definitely related Government procurement operation, the United States Government thereby incurs no responsibility nor abbigation whatsoever; and the fact that the government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data, is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use, or sell any patented invention that may in any way be related thereto.

This report has been reviewed by the Information Office (OI) and is releasable to the National Technical Information Service (NTIS). At NTIS, it will be available to the general public, including foreign nations.

This technical report has been reviewed and is approved for publication.

JOHN W. LINCOLN

AEROSPACE ENGINEER

STRUCTURES DIVISION

DIRECTORATE OF FLIGHT SYSTEMS ENGINEERING

W. Luncola

CLOVIS L. PETRIN, JR. CHIEF, STRUCTURES DIVISION

DIRECTORATE OF FLIGHT SYSTEMS

ENGINEERING

FOR THE COMMANDER

PETER J. BUTKEWICZ, Col, USAF

DIRECTOR

FLIGHT SYSTEMS ENGINEERING

"If your address has changed, if you wish to be removed from our mailing list, or if the addressee is no longer employed by your organization please notify ASD/ENFS __,N-PAFB, OH 45433 to help us maintain a current mailing list".

Copies of this report should not be returned unless return is required by security considerations, contractual obligations, or notice on a specific document.

DISCLAIMER NOTICE

THIS DOCUMENT IS BEST QUALITY PRACTICABLE. THE COPY FURNISHED TO DTIC CONTAINED A SIGNIFICANT NUMBER OF PAGES WHICH DO NOT REPRODUCE LEGIBLY.

READ INSTRUCTIONS BEFORE COMPLETING FORM REPORT DOCUMENTATION PAGE 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALOG NUMBER REPORT NUMBER ASD-TR-80-5036 TYPE OF REPORT & PERIOD COVERED 4. TITLE (and Subtitle) Method for Generating a Randomized Flight-by-Flight Loading Sequence Final Report 6. PERFORMING ORG. REPORT NUMBER for an Aircraft 8. CONTRACT OR GRANT NUMBER(#) 7. AUTHOR(a) John W. Lincoln 10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 9. PERFORMING ORGANIZATION NAME AND ADDRESS Aeronautical Systems Division (ASD/ENFS) Wright-Patterson AFB, OH 45433 12. REPORT DATE 11. CONTROLLING OFFICE NAME AND ADDRESS Aeronautical Systems Division (ASD/ENFS) July 1980 13. NUMBER OF PAGES Wright-Patterson AFB, OH 45433 14. MONITORING AGENCY NAME & ADDRESS(If different from Controlling Office) 18. SECURITY CLASS. (of this report) Unclassified 154, DECLASSIFICATION/DOWNGRADING SCHEDULE 16. DISTRIBUTION STATEMENT (of this Report) Approved for public release, distribution unlimited 17. DISTRIBUTION STATEMENT (of the abetract entered in Block 20, If different from Report) AUPPLEMENTARY NOTES M. HOEFMAN STINFO Officer Flight Systems Engineering 9. KEY WORDS (Continue on reverse side if necessary and identify by block number) Flight-by-Flight Sequence Ground Loads Randomized Loading Temperature Profile Flight Loads 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report provides a technique for obtaining a flight-by-flight loading sequence that could be used in fracture and fatigue analyses and in durability and damage tolerance testing of an aircraft. The major load producing events (i.e. take-off taxi, flight, touch and go landings, landing, and landing taxi) are considered sequentially. The missions in which these events occur can be drawn randomly or put in a predetermined order. The loadings within each event are obtained randomly. The flight loads (include both maneuver loads and gusts) are assumed to be derived from flight recorder data or from a (Con't

DD 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)
DIOCK 20 (CON' L) specific mission profile. In both cases the flight portion is divided into intervals to account for separate phases of the mission and weight changes during flight. In addition an aircraft temperature profile associated with the mission is randomly sampled to provide a flight-by-flight temperature sequence. To provide more flexibility in deriving the flight-by-flight sequence the mission time can be obtained by a random sampling. The computer program for generating the flight-by-flight sequence is included along with a sample problem.

SPECIFITY OF ASSISTEDATION OF THIS PAGE/When Date Enter

FOREWORD

This report was prepared by John W. Lincoln, Structures Division of the Directorate of Flight Systems Engineering. The work was done as a research and development task for general use for generating flight-by-flight loading spectra for aircraft.

	Accession For
	NTIS GRA&I
	DTIC TAB
	Unannounced
	Justification
	Py
DTIC	Aveilability Codes
COPY INSPECTED 2	Avail and/or Dist Special
	H

TABLE OF CONTENTS

SECTION		PAGE
I	INTRODUCTION	1
II	DESCRIPTION OF METHOD	2
III	DESCRIPTION OF COMPUTER PROGRAM	16
	1 NOTATION	16
	2 COMPUTER FLOW DIAGRAM AND PROGRAMS	19
	3 EQUIVALENCE TABLES	21
	4 INPUT DATA	24
	5 SAMPLE PROBLEM	51
APPEND	IX SPECF PROGRAM LISTING	74

٧

LIST OF SYMBOLS

Np	Number of control points on the aircraft structure used in deriving the fatigue test spectrum
N _m	Number of different missions flown by the test aircraft in its life
$\sigma_{R}^{\boldsymbol{a}\boldsymbol{b}}$	Stress at the ath control point for the aircraft resting on its landing gear ready to fly the bth mission.
м <mark>аb</mark> ТТ _р	The number of different stresses in the maximum take-off taxi stress spectrum for the ath control point of an aircraft flying the bth mission
[₫] TT _p	A simple graph, the ordinates of which are members of the maximum take-off taxi stress spectrum for the ath control point of an aircraft flying the bth mission
n a bm TTp	A simple graph whose ordinates are the number of take-off taxi load maximums during one lifetime for the stresses contained in $_{\sigma}^{\rm ab}$ before the mth random sampling $_{\sigma}^{\rm TT}$
$n_{ extsf{TT}}^{ extbf{abm}}$	The sum of the ordinates of n_{TT}^{abm}
nabm TT _p	A simple graph derived from n_{TT}^{abm} whose ordinates are the selection candidates in the prandom sampling process
м <mark>а</mark> b TT _n	The number of different stresses in the minimum take-off taxi stress spectrum for the ath control point of an air-craft flying the bth mission
σ <mark>ab</mark> TT _n	A simple graph, the ordinates of which are members of the minimum take-off taxi stress spectrum for the ath control point of an aircraft flying the bth mission
n ^{abm} TT _n	A simple graph whose ordinates are the number of take-off taxi load minimums during one lifetime for the stresses contained in _ab before the mth random sampling

n <mark>amb</mark> nTT _{nT}	The sum of ordinates of n_{TT}^{abm}
nabm nTT _n	A simple graph derived from n_{TT}^{abm} whose ordinates are the selection candidates in the random sampling process
NS _p	The number of mission intervals (in flight) in the bth mission
Mabc F _p	The number of different stresses in the maximum flight stress spectrum for the ath control point of an aircraft flying the cth mission interval of the bth mission
[⊲] abc [⊲] F _p	A simple graph, the ordinates of which are members of the maximum flight stress spectrum for the ath control point of an aircraft flying the cth mission interval of the bth mission
n <mark>a</mark> bom P	A simple graph whose ordinates are the number of flight load maximums during one lifetime for the stresses contained in abc before the mth random sampling
nabcm F P _T	The sum of the ordinates of negative p
n abcm P p	A simple graph derived from n_F^{abcm} whose ordinates are the selection candidates in the random sampling process
M ^{abc} F _n	The number of different stresses in the negative g flight stress spectrum for the ath control point of an aircraft flying the cth mission interval of the bth mission
σ <mark>a</mark> bc F _n	A simple graph, the ordinates of which are members of the negative g flight stress spectrum for the ath con- trol point of an aircraft flying the cth mission interval of the bth mission
ne n n	A simple graph whose ordinates are the number of flight negative g loads during one lifetime for the stresses contained in gabo before the mth random sampling

nabcm Fn _T	The sum of the ordinates of nabcm
nabcm Fn	A simple graph derived from n _F whose ordinates
	are the selection candidates ^{'N} in the random sampling process
Mabc Fg	The number of different stresses in the one g flight stress spectrum for the ath control point of an aircraft flying the cth mission interval of the bth mission
σ abc Fg	A simple graph, the ordinates of which are members of the one g flight stress spectrum for the ath control point of an aircraft flying the cth mission interval of the bth mission
n abcm F g	A simple graph whose ordinates are the number of flight one g load during one lifetime for the stresses contained in abc before the mth random sampling ${}^\sigma F_g$
n a bcm F g _T	The sum of the ordinates of $n_{\mbox{\scriptsize g}}^{\mbox{\scriptsize abcm}}$
nabcm F	A simple graph derived from $n_{F_{\alpha}}^{abcm}$ whose ordinates
'g	are the selection candidates ^{'g} in the random sampling process
Mab L₁	The number of different stresses in the landing impact stress spectrum for the ath control point of an aircraft flying the bth mission
σ <mark>ab</mark> σ <mark>L i</mark>	A simple graph, the ordinates of which are members of the landing impact stress spectrum for the ath control point of an aircraft flying the bth mission
nLi	A simple graph whose ordinates are the number of landing impact loads during one lifetime for the stresses contained in $\sigma_{\rm L}^{\rm ab}$ before the mth random sampling
nabm Lit	The sum of the ordinates of $n_{L_{\overset{\bullet}{i}}}^{\mbox{abm}}$

/ /

- 1.84 ...

abm	a abm
ηĽ ₁	A simple graph derived from n_L^{abm} whose ordinates are the selection candidates in the random sampling process
Mab LTp	The number of different stresses in the maximum landing taxi stress spectrum for the ath control point of an aircraft flying the bth mission
σ ^{ab} LT _p	A simple graph, the ordinates of which are members of the maximum landing taxi stress spectrum for the ath control point of an aircraft flying the bth mission
nabm LT _p	A simple graph whose ordinates are the number of maximum landing taxi loads during one lifetime for the stresses contained in the ab before the mth random sampling ${}^{\rm CLT}_{\rm p}$
$_{ extsf{nLT}}^{ extsf{abm}}_{ extsf{P}_{ extsf{T}}}$	The sum of the ordinates of n_{LT}^{abm}
nabm LT _p	A simple graph derived from nabm whose ordinates
_,b	are the selection candidates in the random sampling process
Mab LT _n	The number of different stresses in the minimum landing taxi stress spectrum for the ath control point of an aircraft flying the bth mission
oLT _n	A simple graph, the ordinates of which are members of the minimum landing taxi stress spectrum for the ath control point of an aircraft flying the bth mission
nabm LT _n	A simple graph whose ordinates are the number of minimum landing taxi loads during one lifetime for the stresses contained in ab before the mth random sampling
nabm LT _n T	The sum of the ordinates of $n_{LT}^{\mbox{\scriptsize abm}}$

The state of the s

naom nLT _n T	A simple graph derived from n _{LT} whose ordinates
	are the selection candidates in the random sampling process
Mabc F	The number of different temperatures in the flight temperature spectrum for the ath control point of an aircraft flying the cth mission interval of the bth mission
Tabc F	A simple graph, the ordinates of which are members of the flight temperature spectrum for the ath control point of an aircraft flying the cth mission interval of the bth mission
n a bcm F	A simple graph whose ordinates are the number of flight temperature occurrences during one lifetime for the temperatures contained in Tabc before the mth random sampling
nabcm F _T	The sum of the ordinates of n_F^{abcm}
n abcm F	A simple graph derived from n_F^{abcm} whose ordinates are the selection candidates in the random sampling process
м ^{аb} ТG _i	The number of different stresses in the touch-and-go landing impact stress spectrum for the ath control point of an aircraft flying the bth mission
^{ab} ™Gi	A simple graph, the ordinates of which are members of the tough-and-go landing impact stress spectrum for the ath control point of an aircraft flying the bth mission
n <mark>abm</mark> TG _i	A simple graph whose ordinates are the number of touchand-go landing impact loads during one lifetime for the stresses contained in $_{\sigma}^{\rm ab}$ before the mth random sampling $_{\rm TG}^{\rm col}$
nabm TG _i T	The sum of ordinates of n_{TG}^{abm}
nabm ⁿ TG _i	A simple graph derived from nabm whose ordinates are the selection candidates in the random sampling process

${M_{TG}^{ab}}_g$	The number of different stresses in the touch-and-go landing one g stress spectrum for the ath control point of an aircraft flying the bth mission		
gab TGg	A simple graph, the ordinates of which are members of the touch-and-go landing one g stress spectrum for the ath control point of an aircraft flying the bth mission		
nabm TG g	A simple graph whose ordinates are the number of touchand-go landing one g loads during one lifetime for the stresses contained in $_{\mbox{\scriptsize G}}^{\mbox{\scriptsize AB}}$ before the mth random sampling		
nabm TG _{9T}	The sum of ordinates of $n_{\overline{1}G}^{\overline{a}bm}$		
nabm ⁿ TG _g	A simple graph derived from n_{TG}^{abm} whose ordinates are the selection candidates in the $^{\rm g}$ random sampling process		

SECTION I

INTRODUCTION

It is now generally accepted that flight-by-flight fatigue testing is more representative of service experience than block type testing. Further, it appears that load randomization within a flight corresponds reasonably well to flight time history measurements. The purpose of this report is to provide a computer technique to transition from exceedance data for various phases of flight to a randomized flight-by-flight loading sequence.

The method is based on the assumption that the exceedance function for stress at a control point of the aircraft has been stepped (i.e. defined in terms of the number of occurrences at a finite number of stresses). One approach for obtaining the stepped exceedance function is described in reference (1). These data are derived for take-off taxi, flight (including all of the mission interval divisons such as ascent, cruise, combat, loiter, and descent), landing impact, touch-and-go landings, and landing taxi and arranged for input to the computer routine. In addition temperature exceedance functions may be placed in the program to provide a temperature corresponding to each stress occurrence.

It is assumed that the stresses and temperatures are randomized within each phase of flight. The ordering of missions flown within a lifetime may be predetermined or determined randomly. In addition, some freedom is allowed in selecting the flight time in a mission randomly. This feature is useful in the case where the exceedance data are derived from flight recorder data.

In all flight phases, the random sampling is done without replacement. As a consequence, the exceedance function derived from the flight-by-flight load sequence is identical with the input exceedance function.

The computer program along with a sample problem is included. This program terminates at the point of writing the flight-by-flight sequence of loads. To be of practical value, the output of this routine will have to put on cards or tape (whatever is required by the specific requirements of the test set-up).

SECTION II

DESCRIPTION OF METHOD

Based on flight recorder data, or for a new design, the mission profiles, the stress spectrum for positive load factors and the stress spectrum for negative load factors can be computed. The method for doing this was developed in Reference 1. These results when combined with gust, landing, and taxi loads can be used to generate the fatigue test loading sequence.

There are two possibilities that will be considered for this sequence. These are

- Case 1. Stress spectra derived from flight recorder data For this case the basic assumptions are
 - Loading randomized within a specified weight interval and loadings per unit time fixed within an interval
 - Weight intervals treated as nonrandom within a given mission type
 - c. Mission type treated as random or nonrandom within aircraft life
 - d. Hours per flight are randomized
 - e. Temperature treated as random within a given weight interval
- Case 2. Stress spectra derived from the mission profiles
 The basic assumptions are
 - a. Loading randomized within a mission interval and loadings per unit time fixed within a interval
 - Mission intervals treated as nonrandom within a given mission type
 - c. Mission type treated as random or nonrandom within aircraft life
 - d. Hours per flight determined from the appropriate mission profile or randomized
 - e. Temperature treated as random within a given mission interval

For both of these cases the following assumptions will be made

- (a) The sampling of the stress spectra will be done without replacement
- (b) When treated as a random process the mission type will be sampled without replacement

The flight-by-flight fatigue test loading sequence for a specified mission is developed in the following order:

- (a) Aircraft in take-off configuration resting on the landing gear
- (b) Take-off taxi load cycles applied for the time appropriate to this phase. It is assumed that the first load is a maximum, then a minimum followed by a maximum etc. Further, it is assumed the last load is a minimum.
- (c) The flight load cycles are applied mission or weight (as appropriate) interval by interval for the entire flight. The first loading in flight is a maximum. This is followed by a minimum (either from the population of one g load or the population of less than one g loads). The maximum-minimum-maximum etc. sequence is continued throughout the segment. The last flight load in each segment is assumed to be a minimum. As an option, the time spent in a given flight may be selected randomly. A selection may be made for each mission interval (or weight interval) in a mission.
- (d) The landing impact follows the last minimum flight load. This is a one time loading that is derived from a distribution of sink speeds, attitude, etc.
- (e) The final part of the loading sequence is the landing taxi. This is a cyclic loading with the first load a maximum followed by a minimum and then another maximum etc. It is assumed that the last load is a minimum. The time spent in landing taxi is that which is appropriate to the mission specified.

For each flight load occurrence in a mission or weight interval there will be an associated temperature derived from the velocity and altitude variations within that segment. It will be assumed that the population of temperatures is independent of the population of loads. Consequently, the sampling of the temperature population does not depend on the loading that has been selected for that time in the mission.

The following definitions describe the functions required to implement this process.

Suppose each of a, b, Np, and Nm a positive integer such that a is in [1, Np] and b is in [1, Nm]. Further, suppose that $_{\sigma}^{ab}$ is the stress at the ath control point for the aircraft resting on R its landing gear ready to fly the bth mission.

Suppose that M_{TTp}^{ab} is a positive integer and σ_{TTp}^{ab} is a simple graph such that the x-projection of σ_{TTp}^{ab} is the set of integers in [1, M_{TTp}^{ab}] and if i and itl are in [1, M_{TTp}^{ab}] then σ_{TTp}^{ab} is a finite number sequence with x-projection [1, M_{TTp}^{ab}]. Now suppose that i is a positive integer in [1, M_{TTp}^{ab}] and n_{TTp}^{ab} is a simple graph such that the point $(\sigma_{TTp}^{ab}(i)$, n_{TTp}^{ab} $(\sigma_{TTp}^{ab}(i))$ belongs to n_{TTp}^{ab} only if n_{TTp}^{ab} $(\sigma_{TTp}^{ab}(i))$ is the number of take-off taxi load maximums during one lifetime at the stress $\sigma_{TTp}^{ab}(i)$ for the ath control point of the aircraft flying the bth mission. The total number of these take-off taxi load maximums is

$$n_{\overline{T}p_{T}}^{ab1} = \sum_{i=1}^{Mab} n_{\overline{T}p}^{ab1} \quad (\sigma_{\overline{T}p}^{ab}(i))$$

Therefore there are $n_{TT}^{\mbox{\scriptsize abl}}$ selection candidates to obtain the

the first one of the M_{TTp}^{ab} stresses. A selection is made from the population of integers in [1, n_{TT}^{ab}] on the basis that if i and j

are integers in [1, n_{TTp}^{abl}] then the probability of choosing i is equal to the probability of choosing j. Now, suppose that n_{TTp}^{abl} is a simple graph with x-projection zero plus the set of integers in [1, M_{TTp}^{ab}]. Also, n_{TTp}^{abl} (o) = 0 and if i is in [1, M_{TTp}^{abl}] then

$$n_{TTp}^{abl}(i) = \sum_{k=1}^{i} n_{TTp}^{abl} (\sigma_{TTp}^{ab}(k)).$$

Therefore, if j is an integer chosen from the integers in [1, n_{TT}^{ab1}] then there exists a number m such that $n_{TTp}^{ab1}(m-1) < j \le n_{TTp}^{ab1}(m)$.

It is desired to sample the population of integers in [1, $n_{TTp_T}^{ab1}$] without replacement. Therefore, before the second selection of a maximum stress is made the number of maximums at the stress $\sigma_{TTp}^{ab}(m)$ must be reduced by one. Based on this reduction, the simple graphs n_{TTp}^{ab1} and n_{TTp}^{ab1} are transformed into n_{TTp}^{ab2} and n_{TTp}^{ab2} . It follows then if $n_{TTp}^{ab2} = n_{TTp}^{ab1}$ -1 and if j is an integer chosen from the integers in [1, n_{TTp}^{ab2}] then there exists a number m such that $n_{TTp}^{ab2}(m-1) < j \le n_{TTp}^{ab2}(m)$. This process can be repeated until all of the maximums have been selected.

Suppose that M_{TTn}^{ab} is a positive integer and σ_{TTn}^{ab} is a finite number sequence with x-projection [1, M_{TTn}^{ab}]. Now suppose that i is a positive integer in [1, M_{TTn}^{ab}] and n_{TTn}^{ab} is a simple graph such that the point

 $(\sigma_{TTn}^{ab}(i), n_{TTn}^{abl}(\sigma_{TTn}^{ab}(i)))$ belongs to n_{TTn}^{abl} only if $n_{TTn}^{abl}(\sigma_{TTn}^{ab}(i))$ is the number of take-off taxi load minimums during one lifetime at the stress $\sigma_{TTn}^{ab}(i)$ for the ath control point of the aircraft flying the bth mission. The total number of these take-off taxi load minimums is

$$n_{TT}^{abl} = \sum_{i=1}^{Mab} n_{TT}^{abl} (\sigma_{TTn}^{abl}(i)) = n_{TT}^{abl}$$

In this case there are the same number of selection candidates as for the take-off taxi load maximums. The selection from the minimums is made on the same basis as from the maximums. Suppose that n_{TTn}^{abl} is a simple graph with x-projection zero plus the set of integers in [1, M_{TTn}^{ab}]. Further, suppose that $n_{TTn}^{abl}(o) = 0$ and if i is in [1, M_{TTn}^{abl}] then

$$n_{TTn}^{abl}(i) = \sum_{k=1}^{i} n_{TTn}^{abl} (\sigma_{TTn}^{ab}(k))$$

Therefore, if j is an integer chosen from the integers in [1, n_{TT}^{abl}] then there exists a number m such that $n_{TT}^{abl}(m-1) < j \le n_{TT}^{abl}(m)$

As in the case of the maximums it is desired to sample the minimums without replacement. Consequently, the simple graphs $n_{TT_n}^{abl}$ and $n_{TT_n}^{abl}$ are transformed to $n_{TT_n}^{ab2}$ and $n_{TT_n}^{ab2}$, etc.

Suppose that each of c and N_S^b is a positive integer such that c is in [1, N_S^b]. Further, suppose that M_F^{abc} is a positive integer and σ_F^{abc} is a finite number sequence with x-projection [1, M_F^{abc}]. Now, suppose that i is a positive integer in [1, M_F^{abc}] and n_F^{abc} is a

simple graph such that the point $(\sigma_{F_p(i)}^{abc}, n_{F_p}^{abcl}(\sigma_{F_p(i)}^{abc}))$ belongs to $n_{F_p}^{abcl}$ only if $n_{F_p}^{abcl}(\sigma_{F_p(i)}^{abc})$ is the number of flight "positive g loads" during one lifetime at the stress $\sigma_{F_p(i)}^{abc}$ for the ath control point of

the airplane flying the cth interval of the bth mission. The term "positive g loads" refers to those maximum load occurrences corresponding to \mathbf{n}_{z} in excess of one.

The total number of these positive g loads is

$$n_{F_{p_T}}^{abcl} = \sum_{i=1}^{M_{p_T}} n_{F_p}^{abcl} (\sigma_{F_p(i)}^{abc})$$

For the first load selection after take-off there are n_{Fp}^{abl1} selection candidates to obtain one of M_{Fp}^{abl} stresses. A selection is made from the population of integers in [1, n_{Fp}^{abl1}] on an equal probability basis (as for the taxi). Now, suppose that n_{Fp}^{abc1} is a simple graph with x-projection zero plus the set of integers in [1, M_{Fp}^{abc}]. Also, n_{Fp}^{abc1} = 0 and if i is in [1, M_{Fp}^{abc}] then

$$n_{F_p(i)}^{abcl} = \sum_{k=1}^{i} n_{F_p}^{abcl} (\sigma_{F_p}^{abc}(k)).$$

Thus, if j is an integer chosen from the integers in [1, n_F^{abll}] then there exists a number m such that $n_{F_p(m-1)}^{abll} < j \le n_{F_p(m)}^{abll}$.

This population is also sampled segment by segment without replacement until all of the maximums are selected.

Suppose that $M_{F_n}^{abc}$ is a positive integer and $\sigma_{F_n}^{abc}$ is a finite number sequence with x-projection [1, $M_{F_n}^{abc}$]. Further, suppose that i is a positive integer in [1, $M_{F_n}^{abc}$] and $n_{F_n}^{abc}$ is a simple graph such that the point $(\sigma_{F_n}^{abc})$, $n_{F_n}^{abcl}$ $(\sigma_{F_n}^{abc})$) belongs to $n_{F_n}^{abcl}$ only if $n_{F_n}^{abcl}$ $(\sigma_{F_n}^{abc})$ is the number of "negative g loads" during one lifetime at the stress $\sigma_{F_n}^{abc}$ for the ath control point of the airplane flying the cth interval of the bth mission. The term "negative g loads" refers to those minimum load occurrences corresponding to n_z less than one.

The total number of these negative g loads is

$$n_{F_{n_{T}}}^{abcl} = \sum_{i=1}^{M} n_{F_{n}}^{abcl} (\sigma_{F_{n}}^{abc} (i))$$

It is assumed that each positive g loading is followed by either a negative g load or by a "one g load" (a "one g load" is a load corresponding to an n_7 minimum equal to one).

The total number of one g loads for the ath control point of the aircraft flying the cth interval of the bth mission is

$$n_{F_{g_{T}}}^{abcl} = n_{F_{p_{T}}}^{abcl} - n_{F_{n_{T}}}^{abcl}$$

The stress spectrum for the one g loads will be derived from the velocity, altitude, and weight interval load occurrences that were used for the positive g load stress spectrum. It is assumed that for each load occurrence the normal load factor will be equal to one. To obtain the correct number of minimums from this spectrum, the number of loadings at each stress level will have to be multiplied by the ratio $\frac{1}{1000} \frac{1}{1000} \frac{1$

spectrum can be defined as follows:

Suppose M_{Fg}^{abc} is a positive integer and σ_{Fg}^{abc} is a finite number sequence with x-projection the interval [1, M_{Fg}^{abc}]. Also, suppose that i is an integer in [1, M_{Fg}^{abc}] and n_{Fg}^{abc} is a simple graph such that the point $(\sigma_{Fg}^{abc}(i), n_{Fg}^{abc})$ $(\sigma_{Fg}^{abc}(i))$ belongs to n_{Fg}^{abc} only if n_{Fg}^{abc} $(\sigma_{Fg}^{abc}(i))$ is the number of "one g loads" during one lifetime at the stress $\sigma_{Fg}^{abc}(i)$ for the ath control point of the airplane flying the cth interval of the bth mission. Note that

The selection of the flight load minimum is complicated by the fact that it may come from one of the negative g loads or it may come from one of the one g loads. This condition may be handled as follows: Suppose $\max_{n \in \mathbb{R}} \text{ is a simple graph with } x\text{-projection zero plus the set}$

of integers in [1, M_{Fg}^{abc} + M_{Fn}^{abc}]. If i is in [1, M_{Fg}^{abc}] then

$$n_{Fn}^{abcl}$$
 (i) is $\sum_{k=1}^{i} n_{Fg}^{abcl}$ ($\sigma_{Fg}^{abc}(k)$). If i is in

[Mabc + 1, Mabc + Mabc] then
$$\eta_{Fn}^{abc}$$
 (i) is

$$nabcl$$
 + $\sum_{k=1}^{i-M_{Fg}} nabcl$ ($\sigma_{Fn}^{abc}(k)$). Also, $n_{Fn}^{abcl}(o) = o$. Therefore,

for the first flight load minimum selection, if j is an integer chosen from the integers in [1, nable] then there exists a number nable

m such that $n_{Fn}^{ab11}(m-1) < j \le n_{Fn}^{ab11}(m)$. Again, the sampling is made without replacement so that the number of minimums is reduced by one. The transformations of n_{Fg}^{ab11} , n_{Fn}^{ab11} , and n_{Fn}^{ab12} to n_{Fg}^{ab12} , n_{Fn}^{ab12} , and n_{Fn}^{ab12} follows from this reqirement. This population is sampled segment by segment until all of the minimums are drawn.

The landing impact stress spectrum will be sampled once per flight without replacement. This spectrum can be defined as follows: Suppose $M_{L_{i}}^{ab}$ is a positive number and $\sigma_{L_{i}}^{ab}$ is a finite number sequence with x-projection [1, $M_{L_{i}}^{ab}$]. Further, suppose j is a positive integer in [1, $M_{L_{i}}^{ab}$] and $n_{L_{i}}^{ab}$ is a simple graph such that the point $(\sigma_{L_{i}}^{ab}$ (j), $n_{L_{i}}^{ab}$ ($\sigma_{L_{i}}^{ab}$ (j)) belongs to $n_{L_{i}}^{ab}$ only if $n_{L_{i}}^{ab}$ ($\sigma_{L_{i}}^{ab}$ (j)) is the number of landing impact minimums during one lifetime at the stress $\sigma_{L_{i}}$ (j) for the ath control point of the airplane flying the bth mission.

Suppose that $M_{LT_p}^{ab}$ is a positive integer and $\sigma_{LT_p}^{ab}$ is a finite number sequence with x-projection [1, $M_{LT_p}^{ab}$]. Further, suppose that i is a positive integer in [1, $M_{LT_p}^{ab}$] and $n_{LT_p}^{ab1}$ is a simple graph such that the point $(\sigma_{LT_p}^{ab}(i), n_{LT_p}^{ab1})$ $(\sigma_{LT_p}^{ab1}(i))$ belongs to $n_{LT_p}^{ab}$ only if $n_{LT_p}^{ab}$ $(\sigma_{LT_p}^{ab1}(i))$ is the number of landing taxi load maximums during one lifetime at the stress $\sigma_{LT_p}^{ab}(i)$ for the ath control point of the

aircraft flying the bth mission. The total number of these maximums is

$$n_{LT}^{abl} = \sum_{i=1}^{M_{LT}^{ab}} n_{LT}^{abl} (\sigma_{LT}^{ab} (i)).$$

The landing taxi stress selection is analogous to that selection used for the take-off stresses. In this case there are n_{LT}^{abl} selection candidates to obtain the first one of the

 $M_{LT_p}^{ab}$ stresses. This selection is made on an equal probability basis. Now suppose that $\eta_{LT_p}^{abl}$ is a simple graph with x-projection zero plus the set of integers in [1, $M_{LT_p}^{ab}$]. Also, $\eta_{LT_p}^{abl}(o)$ = 0 and if i is in [1, $M_{LT_p}^{abl}$] then

$$n_{LT_p}^{abl}(i) = \sum_{k=1}^{i} n_{LT_p}^{abl} (\sigma_{LT_p}^{ab}(k))$$

The simple graph $n_{LT_p}^{abl}$ is used to determine the stress that corresponds to the selection from the $n_{LT_p}^{abl}$ integers.

Again, the sampling is done without replacement until the entire population has been selected.

Suppose $M_{LT_n}^{ab}$ is a positive integer and $\sigma_{LT_n}^{ab}$ is a finite number sequence with x-projection [1, $M_{LT_n}^{ab}$]. Further, suppose that i is a positive integer in [1, $M_{LT_n}^{ab}$] and $n_{LT_n}^{ab1}$ is a simple graph such that the point $(\sigma_{LT_n}^{ab}(i), n_{LT_n}^{ab1}(\sigma_{LT_n}^{ab}(i)))$ belongs to $n_{LT_n}^{ab1}$ only if $n_{LT_n}^{ab}(\sigma_{LT_n}^{ab1}(i))$ is the number of landing taxi load

minimums during one lifetime at the stress σ_{LT}^{ab} (i) for the ath control point of the aircraft flying the bth mission. The total number of these maximums is

$$n_{LT_{n_T}}^{abl} = \sum_{i=1}^{M_{LT_n}^{abl}} n_{LT_n}^{abl} (\sigma_{LT_n}^{(i)})$$

The minimum stress selection is made on the same basis as the maximum stress selection. For this purpose suppose that n_{LT}^{abl} is a simple graph with x-projection zero plus the set of integers in [1, M_{LT}^{ab}]. Also, n_{LT}^{abl} (o) = 0 and if i is in [1, M_{LT}^{ab}] then

$$n_{LT_n}^{abl}(i) = \sum_{k=1}^{i} n_{LT_n}^{abl} (\sigma_{LT_n}^{ab}(k))$$

The sampling for the minimum stresses is done without replacement until all of the candidates have been selected.

To include the temperature effects on the test, the following functions need to be defined. Suppose that $_{H}^{abc}$ is a positive integer and $_{H}^{abc}$ is a finite number sequence with x-projection [1, $_{H}^{abc}$]. Further, suppose that i is a positive integer in [1, $_{H}^{abc}$] and $_{H}^{abc}$ is a simple graph such that the point $(T_{F}^{abc}(i), n_{F}^{abc}(T_{F}^{abc}(i)))$ belongs to $_{H}^{abc}$ only if $_{H}^{abc}$ ($_{H}^{abc}$ (i)) is the number of occurrences during one lifetime of the temperature $_{H}^{abc}$ (i) at the ath control point of the airplane flying the cth interval of the bth mission.

The total number of these temperature occurrences must agree with the number of load occurrences. That is,

$$n_F^{abcl} = \sum_{i=1}^{M_F^{abcl}} n_F^{abcl} (T_F^{abc}(i)) = 2n_F^{abcl}$$

The temperature sampling is made without replacement first from the set of integers in [1, n_{T}^{abll}]. For this purpose suppose n_{F}^{abcl} is a simple graph with x-projection zero plus the set of integers in [1, M_{F}^{abc}]. Also, $n_{F}^{abcl}(o) = 0$ and if i is in [1, M_{F}^{abcl}] then

$$n_F^{abcl}(i) = \sum_{k=1}^{i} n_F^{abcl} (T_F^{abc}(k))$$

Therefore, if j is an integer chosen from the integers in [1, n_F^{abll}] then there exists a number m such that $T = n_F^{abll}(m-1) < j \le n_F^{abll}(m)$

This population is sampled segment by segment until all temperatures have been selected.

The special case of the touch-and-go landing must be considered. For this case it is assumed that there are two loads. First, there is a landing impact load followed by a "one g" load. The first touch-and-go in a given mission is assumed to be preceded by a flight load minimum. If there are repeated touch-and-go landings it is assumed that there are no flight loads between them.

The required functions for this case are defined as follows: Suppose $_{\text{M}}^{\text{ab}}_{\text{TG}_{i}}$ is a positive integer and $_{\text{G}}^{\text{ab}}_{\text{TG}_{i}}$ is a finite number sequence with x-projection [1, $_{\text{TG}_{i}}^{\text{ab}}$]. Further suppose that j is a positive integer in [1, $_{\text{TG}_{i}}^{\text{ab}}$] and $_{\text{TG}_{i}}^{\text{ab}}$ is a simple graph such that the point $(\sigma_{\text{TG}_{i}}^{\text{ab}}(j), n_{\text{TG}_{i}}^{\text{ab}}(\sigma_{\text{TG}_{i}}^{\text{(j)}}))$ belongs to $n_{\text{TG}_{i}}^{\text{ab}}$ only if $n_{\text{TG}_{i}}^{\text{ab}}$ $(\sigma_{\text{TG}_{i}}^{\text{ab}}(j))$ is the number of touch-and-go landing impact loads during one lifetime at the stress $\sigma_{\text{TG}_{i}}^{\text{ab}}(j)$ for the ath control point of the

aircraft flying the bth mission. The total number of these landing impact loads is

$$n_{TG_{i_{T}}}^{abl} = \sum_{j=1}^{M_{TG_{i}}^{ab}} n_{TG_{i}}^{abl} (\sigma_{TG_{i}}^{ab}(j))$$

Now, suppose that $n_{TG_i}^{abl}$ is a simple graph such that the x-projection of $n_{TG_i}^{abl}$ is zero plus the integers in [1, $M_{TG_i}^{ab}$]. Also, $n_{TG_i}^{abl}$ (o) = 0 and 1f j is in [1, $M_{TG_i}^{ab}$] then

$$n_{TG_i}^{abl}(j) = \sum_{k=1}^{j} n_{TG_i}^{abl}(\sigma_{TG_i}^{ab}(k))$$

The sampling of the population of integers in [1, $n_{TG_i}^{ab1}$] is made the without replacement as in the case of the previously defined normal landing impact.

For the following one g load suppose that M_{TG}^{ab} is a positive integer and σ_{TG}^{ab} is a finite number sequence with x-projection

[1, $M_{TG_g}^{ab}$]. Further, suppose that i is a positive integer in [1, $M_{TG_g}^{ab}$] and $n_{TG_g}^{ab}$ is a simple graph such that the point $(\sigma_{TG_g}^{ab}(i), n_{TG_g}^{ab}(\sigma_{TG_g}(i)))$

belongs to $n_{TG_g}^{abl}$ only if $n_{TG_g}^{abl}$ ($\sigma_{TG_g}^{ab}$ (i)) is the number of one g load conditions (after a touch-and-go landing) during one lifetime at the stress $\sigma_{TG_g}^{ab}$ (i) for the ath control point of the aircraft flying the bth mission.

The total number of these loads must be the same as the touch-and-go impact loads. Therefore

$$n_{TG}^{abl} = \sum_{i=1}^{M_{TG}^{ab}} n_{TG}^{abl}(\sigma_{TG}^{ab}(i)) = n_{TG_{i_{TG}}}^{abl}$$

To fascillitate the sampling process suppose that $\eta_{TG_g}^{abl}$ is a simple graph such that the x-projection of $\eta_{TG_g}^{abl}$ is zero plus the set of integers in [1, $M_{TG_g}^{ab}$]. Further $\eta_{TG_g}^{abl}(o)$ = 0 and if i is in [1, $M_{TG_g}^{ab}$] then

$$n_{TG_g}^{abl}(i) = \sum_{k=1}^{i} n_{TG_g}^{abl}(\sigma_{TG_g}^{ab}(k))$$

The sampling of the population of integers in [1, $n_{TG_g}^{abl}$] is made without replacement.

SECTION III

DESCRIPTION OF COMPUTER PROGRAM

1 NOTATION

- NCASE = 1 if flight maneuver stress spectra is derived from recorded data
 - = 2 if flight maneuver stress spectra is derived from mission profiles

NM - Number of missions

- NRANM = 1 if missions are randomly selected
 - = 2 if mission selection is nonrandom
- NMTMS = 1 if the number of maximum flight load occurrences per mission is nonrandom. If NMTMS >1 then NMTMS is the number of possible candidates for random selection of the number of maximum flight load occurrences per mission
- NFLT Number of flights in one lifetime
- NHRS Number of flight hours in one lifetime
- MISRPT Number of times a mission sequence occurs in a lifetime (for nonrandom mission selection)
- MNUMS Number of different mission selections in a sequence (for nonrandom mission selection)
- NS(i) Number of mission intervals in the ith mission (excluding take-off and landing)
- NTG(i) Number of touch-and-go landings in the ith mission
- NTEMP(i) = 1 if a temperature profile is not included in the ith
 mission
 - = 2 if a temperature profile is included in the ith mission
- NTTF(i) Number of maximum take-off taxi load occurrences per flight for the ith mission
- NFF(k,i,j) Number of maximum flight load occurrences per flight for the kth selection from NMTMS possible candidates for the jth interval of the ith mission
- NLTF(i) Number of maximum landing taxi load occurrences per flight for the ith mission

- MNUM(i) The ith mission number selected (nonrandomly) in a mission sequence that occurs MISRPT times in a lifetime
- NUMRPT(i) The number of entries of MNUM(i) within a mission sequence
- NFRAC(k, i, j) Number of times per lifetime that the kth selection from NMTMS possible candidates for the jth interval of the 1th mission that the number NFF(k, i, j) is selected
- NUMML(i) Number of times the ith mission occurs in one lifetime
- MTTP(i) Number of maximum take-off taxi load intervals for the ith mission
- MTTN(1) Number of minimum take-off taxi load intervals for the ith mission
- MFP(i, j) Number of positive g load intervals for the jth interval of the ith mission
- MFN(i, j) Number of negative g load intervals for the jth interval of the ith mission
- MFG(i, j) Number of one g load intervals for the jth interval of the ith mission
- MLI(i) Number of landing impact load intervals for the ith mission
- MLTP(i) Number of maximum landing taxi load intervals for the ith mission
- MLTN(i) Number of minimum landing taxi load intervals for the ith mission
- MF(i, j) Number of temperature intervals for the jth interval of the ith mission
- MTGI(i) Number of touch-and-go landing impact load intervals for the ith mission
- MTGG(i) Number of touch-and-go landing one g load intervals for the ith mission
- NTTP(1, j) Number of maximum take-off taxi load occurrences in the jth load interval for the ith mission
- NTTN(i, j) Number of minimum take-off taxi load occurrences in the jth load interval for the ith mission
- NFP(i, j, k) Number of positive g load occurrences in the kth load interval for the jth interval of the ith mission

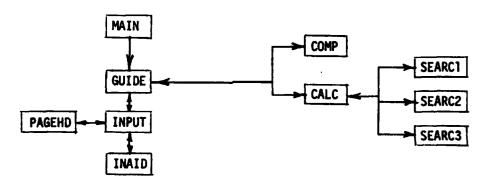
- NFN(i, j, k) Number of negative g load occurrences in the kth load interval for the jth interval of the ith mission
- NFG(i, j, k) Number of one g load occurrences in the kth load interval for the jth interval of the ith mission
- NLI(i, j) Number of landing impact load occurrences in the jth load interval for the ith mission
- NLTP(1, j) Number of maximum landing taxi load occurrences in the jth load interval for the ith mission
- NLTN(i, j) Number of minimum landing taxi load occurrences in the jth load interval for the ith mission
- NF(i, j, k) Number of temperature occurrences in the kth temperature interval for the jth interval of the ith mission
- NTGI(i, j) Number of touch-and-go landing impact load occurrences per lifetime in the jth load interval for the ith mission
- NTGG(i, j) Number of touch-and-go landing one g load occurrences per lifetime in the jth load interval for the ith mission
- TL Temperature for all ground load conditions
- SR(i) Stress for the take-off configuration for the ith mission (aircraft resting on the landing gear)
- STTP(i, j) Stress in the jth maximum take-off taxi load interval for the ith mission
- STTN(i,j) Stress in the jth minimum take-off taxi load interval for the ith mission
- SFP(i, j, k) Stress in the kth positive g flight load interval for the jth interval of the ith mission
- SFN(i, j, k) Stress in the kth negative g flight load interval for the jth interval of the ith mission
- SFG(i, j, k) Stress in the kth one g flight load interval for the jth interval of the ith mission
- SLI(i, j) Stress in the jth landing impact load interval for the ith mission
- SLTP(1, j) Stress in the jth maximum landing taxi load interval for the ith mission
- SLTN(1, j) Stress in the jth minimum landing taxi load interval for the ith mission

- TF(i, j, k) Temperature in the kth flight temperature interval for the jth interval of the ith mission
- STGI(i, j) Stress in the jth touch-and-go landing impact load interval for the ith mission
- STGG(i, j) Stress in the jth touch-and-go one g load interval for the ith mission

2 COMPUTER FLOW DIAGRAM AND PROGRAMS

The computer routine was coded in FORTRAN Extended Language with the main program and subroutines arranged as follows:

SPECF Program (See Appendix A)



- MAIN Main Program Sets NZERO to zero and transfers control to GUIDE
- GUIDE Subroutine Initially zeros input and output numbers and after first case zeros output numbers before the calculations are performed GUIDE is the subroutine for transferring control to INPUT, COMP, and CALC in turn.
- INPUT Subroutine Reads in all input data. The details of the data input are discussed later in this section
- PAGEHD Subroutine Writes out page heading including run identification, date, and page number
- COMP Subroutine Checks the input data for compatibility as follows:

For i in [1, NM]

MTTP(i)

NTTF(i) - NUMML(i) =
$$\Sigma$$
 $i=1$

$$\begin{aligned} & \text{MTTN(i)} \\ & \text{NTTF(i)} \cdot \text{NUMML(i)} &= \sum_{\substack{j=1 \\ j=1}}^{\text{MTTN(i)}} & \text{NTTN(i, j)} \\ & \text{NUMML(i)} &= \sum_{\substack{j=1 \\ j=1}}^{\text{MLI(i)}} & \text{NLI(i, j)} \end{aligned}$$

$$NLTF(i) \cdot NUMML(i) = \sum_{j=1}^{MLI(i)}$$

$$NTG(i) \cdot NUMML(i) = \sum_{j=1}^{MTGI(i)} NTGI(i, j)$$

$$\begin{array}{ccc}
 & \text{NM} \\
 & \text{NFLT} = \Sigma & \text{NUMML(i)} \\
 & \text{i=1}
\end{array}$$

For j in [1, NS(i)]

NMTMS
$$\Sigma$$
 NFF(i, j, k) * NFRAC (i, j, k) = Σ NFP(i, j, k) k=1 NFP(i, j, k)

If any of the above conditions are violated, an error signal will be printed and GUIDE will be called.

CALC - Subroutine - Computes and prints flight-by-flight load sequence

SEARC1 - Subroutine - Makes random selection of stress where the number of occurrences per lifetime is a one dimensional array

SEARC2 - Subroutine - Makes random selection of stress where the number of occurrences per lifetime is a two dimensional array

SEARC3 - Subroutine - Makes random selection of stress of temperature where the number of occurrences per lifetime is a three dimensional array

3 EQUIVALENCE TABLES

All input numbers for this routine are placed in blank common. All input floating point numbers are called parameters and are contained in P (dimensioned 13,000). All input fixed point numbers are called integers and are contained in N (dimensioned 13,500). To make the program usable, EQUIVALENCE statements are used to give the P and N numbers more recognizable names. The SPECF program parameter and integer tables are given below.

EQUIVALENCE TABLE - P (Parameters)

Р	Dim	Term	Р	Dim	Term
3	(1)	TL.	101 1111 115 354 415 654 715 3114 3115 5514 5515 7914 7915 8154 8215 8454 8515 8754 8815 11214 11215 11454 11515 11754 11815 12114	(12) (12,20) (12,20) (12,10,20) (12,10,20) (12,10,20) (12,20) (12,20) (12,20) (12,20) (12,20) (12,20) (12,30) (300) (300)	SR(1) SR(12) STTP (1,1) STTP(12, 20) STTN (1,1) STTN(12, 20) SFP(1, 1, 1) SFP(12, 10,20) SFN(1, 1, 1) SFN(12, 10,20) SFG(1, 1, 1) SLI(12, 20) SLI(1, 1) SLI(12, 20) SLTP(1, 1) SLTN(12, 20) STTP(1, 1) SLTN(12, 20) STGI(1, 1) STGI(12, 20) STGI(1, 1) STGI(12, 20) STGG(1, 1) STGG(12, 20) STRESS(1) STRESS(300) TEMP(1) TEMP(300)

EQUIVALENCE TABLE - N (Integer)

N	Dim	Term	N	Dim	Term
N 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	Dim (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	Term IDENT NPF1 NPF2 NPF3 NPF4 NPF5 NPF6 MONTH DAY YEAR NCASE NM NRANM NMORE NMTMS NFLT NHRS MISRPT MNUMS	115 354 415 654 715 3114 3115 5514 5515 7914 7915 8154 8215 8454 8515 8754 8815 11214 11215 11454 11515 11856 11830	(12, 20) (12, 20) (12, 10, 20) (12, 10, 20) (12, 10, 20) (12, 20) (12, 20) (12, 20) (12, 20) (12, 20) (12, 20) (12, 20) (12, 20) (12, 20) (12, 20) (12, 20)	NTTP(1, 1) NTTP(12, 20) NTTN(1, 1) NTTN(12, 20) NFP (1, 1, 1) NFP(12, 10, 20) NFN(1, 1, 1) NFN(12, 10, 20) NFG(1, 1, 1) NLI(12, 20) NLI(1, 1) NLTP(12, 20) NLTP(1, 1) NLTP(12, 20) NLTN(1, 1) NLTN(12, 20) NF(1, 1, 1) NF(12, 10, 20) NTGI(1, 1, 1) NTGI(12, 20) NTGG(1, 1) NTGG(12, 20) MTTP(1) MTTP(12) MTTP(12)
			11841 11845 11964 11965 12084 12085	(12, 10) (12, 10) (12, 10)	MTTN(12) MFP(1, 1) MFP(12, 10) MFN(1, 1) MFN(12, 10) MFG(1, 1)
48 49	{}	NZERO NPAGE	12204 12205 12216 12220 12231	(12)	MFG(12, 10) MLI(1) MLI(12) MLTP(1) MLTP(12)

EQUIVALENCE TABLE - N - (Integes

N	Dim	Term
12235 12246 12250 12369 12370 12381 12385 12396 12400 12411 12415 12426 12430 12441 12445 12446 12446 12460 12819 12820 12831 12835 12884 12885 12934	(12) (12, 20) (12) (12) (12) (12) (12) (12) (12) (12	MLTN(1) MLTN(12) MF(1, 1) MF(12, 10) MTGI(1) MTGG(1) MTGG(12) MTGG(12) NS(1) NS(12) NTG(1) NTG(12) NTEMP(1) NTFF(12) NTFF(1, 1, 1) NFF(3, 12, 10) NLTF(1) NLTF(12) MNUM(1) MNUM(50) NUMRPT(1) NUMRPT(50)
12935 13294 13295 13306	(3, 12, 10) (12)	NFRAC(1, 1, 1) NFRAC(3, 12, 10) NUMPAL(1) NUMPAL(12)

4 INPUT DATA

All of the input data described below is read into the program by means of the subroutine INPUT. This program is a general purpose routine to read the P (parameters) and N integers. There are several options by which this may be done by this routine. A suggested deck arrangement is given as follows:

14I5 Format

IDENT 1 1 NPF3 0 NPF5 NPF6 MONTH DAY YEAR NCASE NM 515 Format NMTMS NFLT NHRS MISRPT MNUMS 72H Format Run Description	1 NRANM 0
NMTMS NFLT NHRS MISRPT MNUMS 72H Format	T
72H Format	T
72H Format	7
	7
Run Description	7
	1
72H Format	
Run Description	ך
101 100 + NM 1	
6E10.3 Format	
SR(1) - SR(NM)	7
IS Els.7 Format	-
3I5 Format	

1215 Format
NS(1) - NS(NM)
(NS(i) must not exceed 10)
315 Format
12415 12414 + NM 1
12I5 Format
NTG(1) - NTG(NM)
3I5 Format 12430 12429 + NM 1
12I5 Format
NTEMP(1) - NTEMP(NM)
3I5 Format 12445 12444 + NM 1
NTTF(1) - NTTF(NM)
3I5 Format
12820 12819 + NM 1
12I5 Format
NLTF(1) - NLTF(NM)

3I5 Format
13295 13294 + NM 1
12I5 Format
NUMML(1) - NUMML(NM)
If NRANM = 1 go to (bb), if NRANM = 2 go to (aa)
315 Format
(aa) 12835 12834 + MNUMS 1 1215 Format
MNUM(1) - MNUM(MNUMS)
315 Format 12885 12884 + MNUMS 1 1215 Format
NUMRPT(1) - NUMRPT(MNUMS)
(bb) 3I5 Format 11815 11814 + NM 1
12I5 Format
MTTP(1) - MTTP(NM)
(MTTP(i) must not exceed 20)
3I5 Format
11830 11829 + NM 1
12I5 Format
MTTN(1) - MITN(NM)
(MTTN(1) must not exceed 20)

1

12205

MLI(1) - MLI(NM)

12204 + NM

315 Format 12220 12219 + NM 12I5 Format MLTP(1) - MLTP(NM) 3I5 Format 12235 12234 + NM 12I5 Format MLTN(1) - MLTN(NM) If i is in [1, NM] and NTG(i) = 0 go to (b), otherwise go to (a) (a) 315 Format 12370 12369 + NM 12I5 Format MTGI(1) - MTGI(NM)

(MTGI(i) must not exceed 20)

315 Format 12385 12384 + NM1 12I5 Format MTGG(1) - MTGG(NM) (MTGG(i) must not exceed 20) **I5 Format** (b) NM 715 Format 115 MTTP(1) 12 20 6E10.3 Format STTP(1, 1) - STTP(1, MTTP(1)) 715 Format 115 MTTP(i) 12 20 6E10.3 Format STTP(1, 1) - STTP(1, MTTP(1))

715 Format

1 NM MTTP(NM) 1 12 20

6E10.3 Format
STTP(NM, 1) - STTP(NM, MTTP(NM))

115

15 Format NM 715 Format MTTN(1) 415 12 20 6E10.3 Format STTN(1, 1) - STTN(1, MTTN(1)) 715 Format MTTN(i) 20 415 12 6E10.3 Format STTN(i, 1) - STTN(i, MTTN(i)) 715 Format MTTN(NM) 20 415

6E10.3 Format

STTN(NM, 1) - STTN(NM, MTTN(NM))

I5 Format

NM Σ NS(1) i=1

715 Format

	715	1	1	MFP(1, 1)	12	10	20
ı							

```
6E10.3 Format
SFP(1, 1, 1) - SFP(1, 1, MFP(1, 1))
                        715 Format
715
                    MFP(i,j)
                              12
                                      10
                                             20
                        6E10.3 Format
SFP(i, j, 1) - SFP(i, j, MFP(i, j))
                        715 Format
                       MFP(NM, NS(NM)
715
               NS(NM)
                                       12
                                              10
                        6E10.3 Format
SFP(NM, NS(NM),1) - SFP(NM, NS(NM), MFP(NM, NS(NM))
I5 Format
    NS(1)
```

	715 Format							
3115	1	1	MFN(1, 1)	12	10	20		

SFN(1, 1,1) - SFN(1, 1, MFN(1, 1))

6E10.3 Format

715 Format 3115 MFN(1, j) 20 12 10

6E10.3 Format SFN(i, j, 1) - SFN(i, j, MFN(i, j))715 Format 3115 NS(NM) MFN(NM, NS(NM)) 12 10 20 6E10.3 Format SFN(NM, NS(NM), 1) - SFN(NM, NS(NM), MFN(NM, NS(NM)) I5 Format NS(i) i=1 715 Format 5515 MFG(1, 1)12 10 20 6E10.3 Format SFG(1, 1, 1) - SFG(1, 1, MFG(1, 1))715 Format MFG(i, j) 5515 12 10 20 6E10.3 Format SFG(i, j, 1) - SFG(i, j, MFG(i, j))715 Format 5515 NM NS(NM) MFG(NM, NS(NM)) 12 20

6E10.3 Format

SFG(NM, NS(NM), 1) - SFG(NM, NS(NM), MFG(NM, NS(NM))

15 Format

NM Σ NS(1) (NTEMP(1) -1) i=1

If this card entry = 0, omit and go to (d), otherwise go to (c).

(c) 715 Format

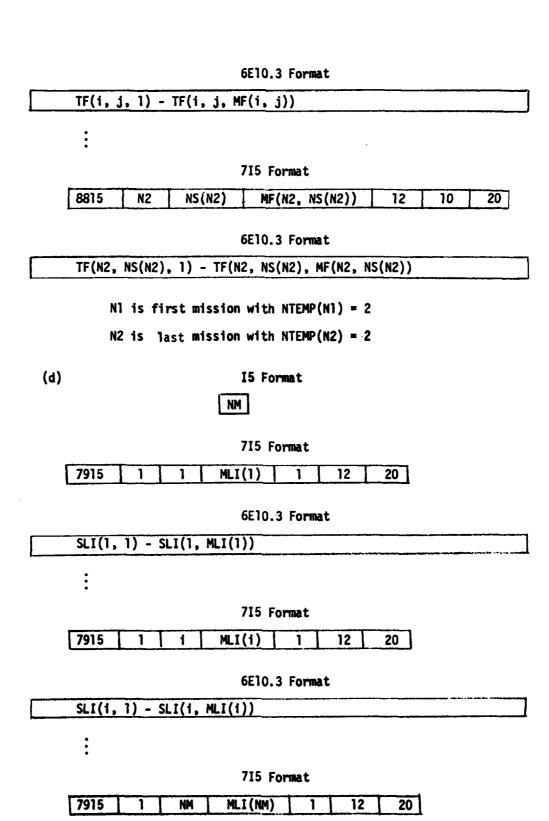
8815 N1 NS(N1) MF(N1, NS(N1)) 12 10 20

6E10.3 Format

TF(N1, NS(N1), 1) - TF(N1, NS(N1), MF(N1, NS(N1))

715 Format

8815 1 j MF(1, j) 12 10 20



6E10.3 Format

SLI(NM, 1) - SLI(NM, MLI(1))

I5 Format

NM

715 Format

8215	1	1	MLTP(1)	1	12	20

6E10.3 Format

SLTP(1, 1) - SLTP(1, MLTP(1))

715 Format

8215 1 1 MLTP(1) 1 12 20

```
6E10.3 Format
SLTP(i, 1) - SLTP(i, MLTP(i))
                        715 Format
                      MLTP(NM)
8215
               NM
                                         12
                                                20
                        6E10.3 Format
SLTP(NM, 1) - SLTP(NM, MLTP(NM))
             I5 Format
           NM
                        715 Format
                     MLTN(1)
8515
                                       12
                                              20
                        6E10.3 Format
SLTN(1, 1) - SLTN(1, MLTN(1))
                        715 Format
8515
                     MLTN(i)
                                       12
                                               20
                        6E10.3 Format
SLTN(i, 1) - SLTN(i, MLTN(i))
                        715 Format
                      MLTN(NM)
8515
               NM
                                                20
```

SLTN(NM, 1) - SLTN(NM, MTLN(NM))

6E10.3 Format

N3 is the number of missions that have a touch-and-go landing. If N3 = 0 omit this card and go to (f), otherwise go to (e). (e) 715 Format 11215 **N4** MTGI (N4) 12 20 6E10.3 Format STGI(N4, 1) - STGI(N4, MTGI(N4)) 7I5 Format 11215 MTGI(i) 12 20 6E10.3 Format STGI(i, 1) - STGI(i, MTGI(i)) 715 Format 11215 12 20 N5 MTGI (N5) 1 6E10.3 Format STGI(N5), 1) - STGI(N5, MTGI(N5))

I5 Format

N3

N4 is first mission with NTG(N4) \neq 0 N5 is last mission with NTG(N5) \neq 0

15 Format

N3

715 Format
11515 1 N4 MTGG(N4) 1 12 20
6E10.3 Format
STGG(N4, 1) - STGG(N4, MTGG(N4))
:
715 Format
11515 1 i MTGG(i) 1 12 20
6E10.3 Format
STGG(i, 1) - STGG(i, MTGG(i))
:
7I5 Format
11515 1 N5 MTGG(N5) 1 12 20
6E10.3 Format
STGG(N5, 1) - STGG(N5, MTGG(N5))
(f) I5 Format
NM · NMTMS
715 Format
12460 1 1 NS(1) 3 12 10
12I5 Format
NFF(1, 1, 1) - NFF(1, 1, NS(1))
:
7I5 Format
12460 1 j NS(j) 3 12 10

12I5 Format
NFF(1, j, 1) - NFF(1, j, NS(3))
:
•
715 Format
12460 NMTMS NM NS(NM) 3 12 10
12I5 Format
NFF(NMTMS, NM, 1) - NFF(NMTMS, NM, NS(NM))
I5 Format
NM-NMTMS
715 Format
12935 1 1 NS(1) 3 12 10
12I5 Format
NFRAC(1, 1, 1) - NFRAC(1, 1, NS(1))
:
715 Format
12935 i j NS(j) 3 12 10
12I5 Format
NFRAC(1, j, 1) - NFRAC(1, j, NS(j))
•
715 Format
12935 NMTMS NM NS(NM) 3 12 10

12I5 Format

NFRAC(NMTMS, NM, 1) - NFRAC(NMTMS, NM, NS(NM))

CHARLES MADE TO SERVICE

I5 Format MM 715 Format 115 MTTP(1) 12 20 12I5 Format NTTP(1, 1) - NTTP(1, MTTP(1)) 715 Format 115 MTTP(i) 12 20 12I5 Format NTTP(i, 1) - NTTP(i, MTTP(i)) 715 Format 115 MM MTTP(NM) 12 20 12I5 Format NTTP(NM, 1) - NTTP(NM, MTTP(NM)) **I5 Format**

415 1 1 MTTN(1) 1 12 20

NM

· ·
12I5 Format
NTTN(1, 1) - NTTN(1, MTTN(1))
•
<u>. </u>
415 1 i MTTN(i) 1 12 20
12I5 Format
NTTN(i, 1) - NTTN(i, MTTN(i))
•
415 1 NM MTTN(NM) 1 12 20
2025 5
12I5 Format
NTTN(NM, 1) - NTTN(NM, MTTN(NM))
I5 Format
NM Σ NS(i)
i=l
715 Format
715 1 1 MFP(1, 1) 12 10 20
713 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
12I5 Format
NFP(1, 1, 1) - NFP(1, 1, MFP(1, 1))
:
•

MFP(1, j)

715 Format

12I5 Format

NFP(i, j, 1) - NFP(i, j, MFP(i, j))

:

715 Format

715	NM	NS(NM)	MFP(NM, NS(NM))	12	10	20

12I5 Format

NFP(NM, NS(NM), 1) - NFP(NM, NS(NM), MFP(NM, NS(NM))

I5 Format

NM Σ NS(i) i=1

715 Format

2226	•		1451/3	• •			
1 3115		1 1	MFN(1.	11	1 17 I	1 133 3	ו מכיו
00		•		.,		, ,,	

1215 Format

NFN(1, 1, 1) - NFN(1, 1, MFN(1, 1))

:

715 Format

3115	i	j	MFN(i, j)	12	10	20

12I5 Format

NFN(i, j, 1) - NFN(i, j, MFN(i, j))

:

715 Format

3115 NM NS(NM) MFN(NM, NS(NM)) 12 10 20

12I5 Format

NFN(NM, NS(NM), 1) - NFN(NM, NS(NM), MFN(NM, NS(NM))

I5 Format

NM Σ NS(i) i=1

715 Format

5515 1 1 MFG(1, 1) 12 10 20

12I5 Format

NFG(1, 1, 1) - NFG(1, 1, MFG(1, 1))

:

715 Format

5515 i j MFG(i, j) 12 10 20

12I5 Format

NFG(i, j, 1) - NFG(i, j, MFG(i, j))

:

715 Format

5515 NM NS(NM) MFG(NM, NS(NM)) 12 10 20

12I5 Format

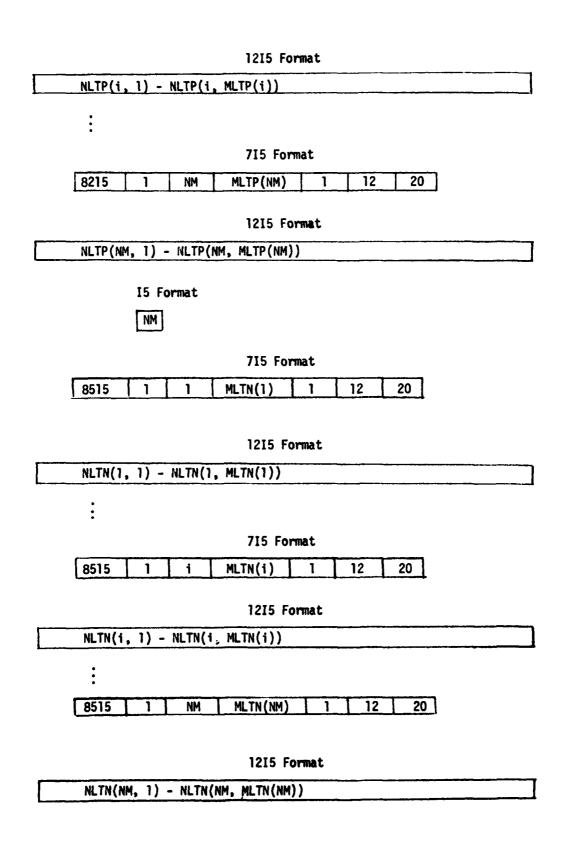
NFG(NM, NS(NM), 1) - NFG(NM, NS(NM), MFG(NM, NS(NM))

15 Format

MM

715 Format
7915 1 1 MLI(1) 1 12 20
12I5 Format
NLI(1, 1) - NLI(1, MLI(1))
:
715 Format
7915 1 i MLI(i) 1 12 20

12I5 Format
NLI(1, 1) - NLI (1, MLI(1))
:
715 Format
7915 1 NM MLI(NM) 1 12 20
7913 1 WH PILI(NH) 1 12 20
12I5 Format
NLI(NM, 1) - NLI(NM, MLI(NM))
15 Format
NM .
7I5 Format
8215 1 1 MLTP(1) 1 12 20
1215 Format
NLTP(1, 1) - NLTP(1, MLTP(1))
•
 -
715 Format
8215 1 i MLTP(1) 1 12 20



15 Format

NM Σ NS(i)(NTEMP(i) - 1) i=1

If this card entry = 0 omit and go to (h) otherwise go to (g)

(g) 715 Format

8815 N1 NS(N1) MF(N1, NS(N1)) 12 10 20

12I5 Format

NF(N1, NS(N1), 1) - NF(N1, NS(N1), MF(N1, NS(N1))

:

715 Format

8815 i j MF(i, j) 12 10 20

12I5 Format

NF(i, j, 1) - NF(i, j, MF(i, j))

:

715 Format

8815 N2 NS(N2) MF(N2, NS(N2)) 12 10 20

1215 Format

NF(N2, NS(N2), 1) - NF(N2, NS(N2), MF(N2, NS(N2))

N1 is first mission with NTEMP(N1) = 2

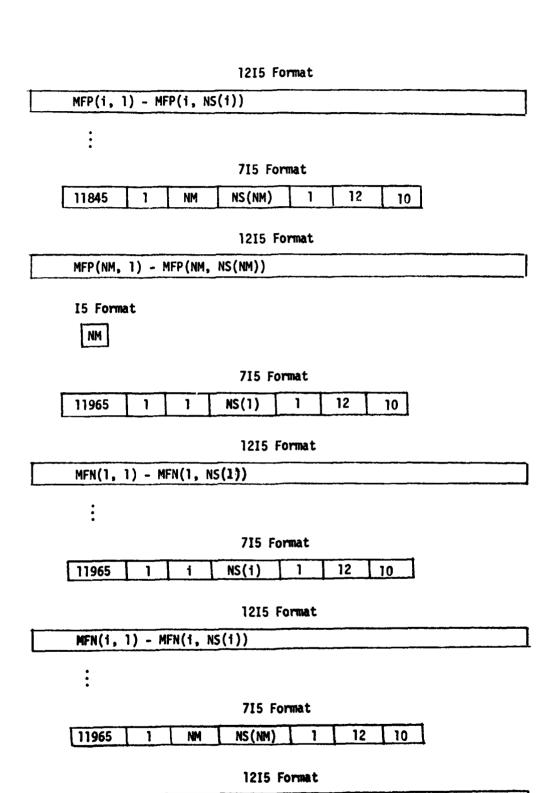
N2 is last mission with NTEMP(N2) = 2

(h) **I5 Format** N3 N3 is the number of missions that have a touch-and-go landing. If N3 = 0 omit this card and go to (j) otherwise go to (i). (i) 715 Format 11215 **N4** MTGI (N4) 12 20 12I5 Format NTGI(N4, 1) - NTGI(N4, MTGI(N4)) 7I5 Format 11215 12 20 MTGI(i) 1215 Format NTGI(1, 1) - NTGI(1, MTGI(1)) 715 Format 11215 N5 MTGI (N5) 12 20 1215 Format NTGI(N5, 1) - NTGI(N5, MTGI(N5)) N4 is first mission with NTG(N4) \neq 0 N5 is last mission with NTG(N5) \neq 0

I5 Format

N3

7I5 Format
11515 1 N4 MTGG(N4) 1 12 20
JOYE Comment
12I5 Format
NTGG(N4, 1) - NTGG(N4, MTGG(N4))
:
7I5 Format
11515 1 i MTGG(i) 1 12 20
12I5 Format
NTGG(i, 1) - NTGG(i, MTGG(i))
•
715 Format
11515 1 N5 MTGG(N5) 1 12 20
1215 Format
NTGG(N5, 1) - NTGG(N5, MTGG(N5))
(j) I5 Format
NM
715 Format
11845 1 1 NS(1) 1 12 10
12I5 Format
MFP(1, 1) - MFP(1, NS(1))
715 Format
11845 1 1 NS(1) 1 12 10



A STATE OF THE STA

MFN(NM, 1) - MFN(NM, NS(NM))

I5 Format NM 715 Format NS(1) 12085 12 10 1215 Format MFG(1, 1) - MFG(1, NS(1))715 Format (i)2N 10 12085 12 12I5 Format MFG(1, 1) - MFG(1, NS(1)) 715 Format NS(NM) 12 12085 NM 12I5 Format MFG(NM, 1) - MFG(NM, NS(NM)) **I5 Format** (NTEMP(1) - 1)1=1

If this entry = 0 omit and go to (1) otherwise go to (k)

12I5 Format

MF(N1, 1) - MF(N1, NS(N1))715 Format 12250 NS(1) 12 10 12I5 Format MF(i, 1) - MF(i, NS(i))715 Format 12250 N2 NS(N2) 12 10 12I5 Format MF(N2, 1) - MF(N2, NS(N2))N1 is first mission with NTEMP(N1 = 2N2 is last mission with NTEMP(N2) = 2(1) END OF FILE The first card contains fourteen (14) fixed point (integer) numbers arranged in 15 fields. These entries are (1) IDENT - run number

(2) 1

(3) 1

(4) 11 + 2N + 2L

N = 1 if i is in [1, NM] and NTG(i) $\neq 0$

N = 0 otherwise

L = 1 if NRANM = 2

L = 0 1f NRANM = 1

(5) 0

- (7) 13 + 2M + 2N
- (8) MONTH
- (9) DAY
- (10) YEAR
- (11) NCASE
- (12) NM
- (13) NRANM
- (14) 0

The second card contains 515 fields with the following entries

- (1) NMTMS
- (2) NFLT
- (3) NHRS
- (4) MISRPT
- (5) MNUMS

The third and fourth cards contain run descriptive information as desired by the user.

The fifth and subsequent cards are arranged as shown above.

5 SAMPLE PROBLEM

A sample run is included to acquaint the user with the input deck arrangement and the output listing. The case considered is an aircraft with a lifetime of twelve hours that is comprised of six flights. There are two missions and the mission time and the mission selection is random. A temperature profile is included in mission 1 and both missions contain touch-and-go landings. The input data and the output listing are given below.

1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	12 1 1 1 1 1 1 1 1 1	-	-	- 7/41/
	12001,		TEST LASE FUN FLIG	TATAO
		101	V PSI TEMP, IN DEGREES F	FOURTH 1
1240 1240		•	Address of the Court of the Cou	The same of the sa
15 15 15 15 15 15 15 15	13 1 2 2 2 2 2 2 2 2 2			The state of the s
124 124	1223 123 1	15000		97
		1946)		
120012112 120012			والمرابعة والمرا	N/6 2
1229, 1220 12 12 12 12 12 12 12	120 120	1	eren der	
	1209 1240	- 1		N16AP &
1205 1202	1205 1200		19	A COMPANY OF THE PARTY OF THE P
120011200	1220,1120,	•		
				11. 15
		13951	THE CONTRACT	NOTE:
1223/1240		~	THE REPORT OF THE PERSON AND THE PER	SUMMENT AND THE PROPERTY OF TH
12235412400 12	1223/31220	ł		
1223/12321	1223/1222	,		
122341236	1235/26.0			1134 b
1223/1222		~		
1235 1222 1 1 1 1 1 1 1 1	1235 1222 1 2 2 2 2 2 2 2			
123541236	123341236	- 1	19	1 1 6
1233412236 123141236 123141236 123141236 123141236 133141236 13415 135141236 13616 13716 1	1235412246 123741224	ונפקרו	76	
1234/1236	133 13 1 2 1 2 2 2 2 2 2 2	1	The same of the sa	The Control of the Co
1235 1235	1235/1247 1235/1247 1 1 1 1 1 1 1 1 1			
	1355412466		The second secon	1018
13 1 2 1 2 2 2 2 2 2 2	1334 13			Mici Z
13 1 2 12 20	115 1 2 20 20 2 2 1 1 2 20 20 2 2 1 2 1 2 20 2 2 2 2			1 991
115 1 15 20	115		An employed in a special control of the second of the seco	#100 miles of the control of the con
		,		3116
	2000, 7 -7007, 0 -200	1000	24 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
			2 . 3 . 1 . 1 . 2	SITE AND
2400.6 -2000.0 -11000.0 -1200.0 -0 -1000.0 -1000.0 -0 -	2500.5006.0 -110.0.6 -120.0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-6000	-7767.c -4600A.6	3116
2000-0000-011000-012000-00	1	~	and the second s	7
2000.0 -000.0 -110.0 -12000.0	2-1640.6	\$10	1 2 [12	5 TA S TO THE RESERVE THE PROPERTY OF THE PROP
25000.0 1.000.0 -11000.0 -1200	2500.0	0000	0.0000	N A L
2500.0 2100.0 2 12 10 20 20 20 21 21 2 10 20 20 20 21 21 2 10 20 20 21 21 2 2 2 2	2500.0 2100.0 2 12 10 20 20 20 20 20 20 20 20 20 20 20 20 20	2396	02 20 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	A TABLE TO A TOTAL OF
2500.0 2700.0 2 25 10 20 20 21 21 2 20 20 20 20 20 20 20 20 20 20 20 20 2	2500.6. 2700.0. 2 12 10 20 20 20 20 20 20 20 20 20 20 20 20 20		200000	
2500, 0 2100, 0 2 17 10 20 711, 1 200, 0 100, 0 100, 0 20 715, 2 200, 0 2 100, 0 2 17 10 20 24000, 2 2200, 0 2500, 0 3000, 0 20 24000, 2 2000, 0 2500, 0 3000, 0 20 24000, 2 2000, 0 2500, 0 3000, 0 20 24000, 2 2000, 0 2500, 0 3000, 0 20 24000, 2 2000, 0 2500, 0 3000, 0 20 24000, 2 2000, 0 2500, 0 3000, 0 20 24000, 2 2000, 0 2000, 0 2000, 0 2000, 0 200 24115, 1 2 12 2 17 10 20 2500, 0 2000, 0 2 17 10 20 2500, 0 2000, 0 2 17 10 20 2500, 0 2000, 0 2 17 10 20 2500, 0 2000, 0 2 17 10 20 2500, 0 2000, 0 2 17 10 20 2500, 0 2000, 0 2 17 10 20 2500, 0 2000, 0 2	3500.0 21000.0 2 12 10 20 711 1 20 20 713 1 20 20 12 10 20 713 2 2000.0 31000.0 20 713 2 2000.0 12 10 20 713 2 2000.0 12 10 20 713 2 2000.0 2000.0 20 713 2 2 2 12 10 20 713 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	. 314	10 10 10 10 10 10 10 10 10 10 10 10 10 1	35
711 1 2 2 17 10 20 C1	2006;6 2006;0 31200;0 20 20 20 20 20 20 20 20 20 20 20 20 20	25000.	27000.0	
26505.6 2605.0 3 10 20 20 20 20 20 20 20 20 20 20 20 20 20	2556.9 280.0.0 10.20 20 CI 2556.9 28050.0 11076.0 10 20 2506.5 12.0.0.0 12 10 20 2400.0 2500.0 2500.0 20 2400.0 2500.0 2500.0 20 2400.0 12.0 20 2400.0 12.0 20 2500.0 12.0 20 2500.0 12.0 20 2500.0 12.0 20 2500.0 12.0 20 2500.0 12.0 20 2500.0 12.0 20 2500.0 12.0 20 2500.0 12.0 20 2500.0 12.0 20 2500.0 12.0 20 2500.0 12.0 20 2500.0 12.0 20 2500.0 12.0 10 20 2500.0 10 20 2500.0 12.0 10 20 2500.0 12.0 10 20 2500.0 12.0 10 20 25	316	02 01 2 2	7 446
2000.0 2 2000.0 2 10 20 20 20 20 20 20 20 20 20 20 20 20 20	20500.0 2000.0 11000.0 20 2000.0 2000	20000	4.0000	2 6 95
2000, 5 3200, 0 3100, 0 50 2000, 5 3200, 0 12 16 20 2000, 2000, 2000, 0 12 10 20 5115 1 15 2 17 10 20 5500, 7 5500, 12 10 20 5115 1 1 3 12 10 20 5115 1 1 3 12 10 20 5115 1 1 3 12 10 20 5115 1 1 3 12 10 20 5115 1 1 3 12 10 20 5115 1 1 3 12 10 20 5115 1 1 3 12 10 20 5115 1 1 3 10 20 5115 1 1 3 10 20 5115 1 1 3 10 20 5115 1 1 3 10 20 5115 1 1 3 10 20 5115 1 1 3 10 20 5115 1 1 3 10 20 5115 1 1 3 10 20 5115 1 1 3 10 20 5115 1 1 3 10 20 5115 1 1 3 10 20 5115 1 3 10 20 5115 1 1 3	2406, 5 3200, 0 3100, 0 80 2406, 5 3200, 0 17 10 20 3405, 7 2 2 10 10 20 20 3115 1 2 10 20 20 5500, 0 7500, 0 17 10 20 5500, 0 17 10 10 10 10 10 10 10 10 10 10 10 10 10		1 2 10 20	• 0.40
24046,5 12246,0 12 16 26 24 24 24 24 24 24 24 24 24 24 24 24 24	24000,5 32200,0 12 10 20 24000,1 22000,0 26500,0 30000,0 3115 1 2 2 10 20 3115 1 2 2 10 10 20 3115 1 2 2 10 10 20 3115 1 2 3 3 2 10 10 20	2000	0°010°00°00°00°00°00°00°00°00°00°00°00°0	ender and and an enter a constant and an enter of the second and an enter o
2400,0 2000,0 2000,0 3000,0 20 215 10 20 20 215 11 2 10 20 20 215 11 2 10 20 20 20 20 20 20 20 20 20 20 20 20 20	2400.0. 25000.0 26500.0 3115	2000	V V V V V V V V V V V V V V V V V V V	CONTRACTOR OF THE PROPERTY OF
2.600.0 2.000.0 2.0500.0 30000.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 + 5000, n 2 + 5000, n 30000, 0 1 1 2 1 2 2 1 2 1 2 2 1 2 1 2 1 2 1 2		20 S S S S S S S S S S S S S S S S S S S	121
7566, 6 706, 6 70 70 70 70 70 70 70 70 70 70 70 70 70	1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	2+000.	20000.0 20500.0 30000.0	The second secon
1) 2 15 10 20 1 1 1 1 1 1 2 1 2 1 1 1 1 2 1 2 1	1 2 12 10 20 1 2 2 12 10 20 1 2 2 12 10 20 1 2 3 12 10 20	•		NAME OF THE PERSON OF THE PERS
1 7500,0 2 15 16 26 1 1 20 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	7500,0 0,000,0 10 20 20 21 7 3 20 20 21 7 3 20 20 21 7 3 20 20 20 20 20 20 20 20 20 20 20 20 20	3115	1 1 3 12 10	
1 3500.0 1 2 12 10 20 CI	1 35 05 10 50 CI	0.000	7600.0 0000.0	245
17 92 91 61 2 6 1	1,200, 1 2 19 10 20	1112	02 01 21 2 2	20 A C
	1	0.000	9,0067	330 mm - T
		SIL	1 3 6 17 10 60	

Contraction of the same

1916 1916	
2515 1 2 10 20 2 10 10 20 20 20 20 20 20 20 20 20 20 20 20 20	
\$515 \$5400 \$5400 \$5515 \$5515 \$5515 \$5515 \$5515 \$5515 \$5515 \$5515 \$5500 \$5515 \$5500 \$5515 \$5500 \$5515 \$5500 \$55	
100 100 10 10 10 10 10	
18900.6 1100.6 1200.0 20 20 20 20 20 20 20 20 20 20 20 20 20	
\$1000.0. \$100.0. \$12.0.0.0. \$20.0.0.0. \$20.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	
15 15 15 16 20 20 20 20 20 20 20 2	
\$515, \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	
1910	
200, 200, 200, 200, 200, 200, 200, 200,	
1 2 2 2 2 2 2 2 2 2	
1 2 2 20 20 20 20 20 2	
1 12 20 60 61 1 1 1 1 2 20 61 1 1 1 1 2 20 61 1 1 1 1 1 2 20 61 1 1 1 1 1 2 20 61 1 1 1 1 1 2 20 61 1 1 1 1 1 2 20 61 1 1 1 1 1 2 20 61 1 1 1 1 1 1 2 20 61 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
1 2 20 20 21 2 20 20 2	
1 12 20 (1 5 5 5 5 5 5 5 5 5	
1 1 2 2 2 3 3 3 3 3 3 3	
1 1 2 2 2 3 3 3 3 3 3 3	
100000	
100,00 - 3 - 200,00 - 1 - 20 - 20 - 20 - 20 - 20 - 20 - 2	
100,00 - 100	
1 1 2 20 21 2 20 21 2 20 21 2 20 21 2 20 21 2 20 21 2 20 21 2 20 21 2 20 21 2 20 21 2 20 21 2 20 21 2 20 21 2 20 21 2 20 20	
1 1 1 2 20	
100,00 -11600,00 -1 12 -20 -1 18 -20	
100000 1100000 1 1 2 20	
100000 -1100000 -1100000 -1000000 -1000000 -1000000 -100000 -100000 -100000 -100000 -100000 -100000 -100000 -100000 -1	
0.000,0 -1.000,0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
2 1 1 2 20 C1 3 2 2 1 1 2 20 C1 3 2 2 1 1 2 20 C1 3 2 2 1 1 1 1 1 1 1 2 20 C1 3 2 3 1 2 2 0 C1 3	
1 1 1 2 20 CI 8 -1956450	
10 02 21 1 2 20 10 10 10 10 10 10 10 10 10 10 10 10 10	
1 2 2 1 2 2 2 3 3 3 3 3 3 3	*
1 1 1 2 20 CT 8	
1 1 1 2 20 CT 8	
1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	The state of the s
02 21 1 2 2 1 1 2 2	
0,0000	
2 340 17	~
1200	
12400 2 1 3 12 10	
12400 2 2 3 12 10	**************************************
	•
12 10 CT NPRAC 2	
NP PAC 3	

auge.		WFRAC 4
-		27 12
12015	2 2 3 12 10	EXPECT OF THE PROPERTY OF THE
		47.850
-		NEDIC 0
~		2179
115	92 21 1 2 1	
	The second of th	
115	1 2 3 1 12 26	
		- 1
~ !		The state of the s
610		Z
		2 CHZ
		ž
,		- a.u.2
3		
	96 07	9
4.5		
		A
100	12 (a 20)	6 44
		0
	12 01 51 6 5	0 d d l R
		Z
2112	7 12 18 28	2 248
		z.2
3115	1 2 2 12 10 20	ż
~		5 N.S.
2115	1 2 12 10 20	
2 5111	02 01 21 2 1 2	7.57
		NEW TO SEE THE PROPERTY OF THE
2112	A5 11 21 2 3	N. W.
2525	10 20 10 20	
-		5 240
5185	2 1 12 10 29	942.10
•		200
3513	2 15 16 20	
-		
5515	1 15 10 60	11 S
		91 93. 10
2000	7 N 31 C 2	
. 3186	2	
7015	1 2 2	I NE I
		ŧ
~		
\$120	. 02 21 1 5 1	2 d1% 1
	~	
3215	92 21 1 2 4 1	4 1 N 10
01		
~		NIN I

	The second of th	
	TO AN TAIL TO THE	

15 5		
1 2 15	20 0, SO 0,	The second of the second secon
		the contract of the property of the contract o
34 1 12	1) \$0 07 CI	The second secon
A615 1 3 3 12	10 20	
16 2 7		
31316	161W 15	
	75	
11215 1 2 2 1	12 20 CI NIGI	
	CI NIGG.	
•	100	to design the same track before the contract of the same of the sa
11515 1 2 4 1	12 80 LI NIGG	
	991X	
1	12 10 51 10	
2 " 2	LE 10 CI MFP	
1 .		
-	12 10 CI #PN 2	
	N.J.	
		AND A COMMAND AND IN THE PROPERTY OF THE PROPE
!		
12065	12 19 CI #F6 Z	
	94	
-		A THE THE PROPERTY AND THE TAX AND A RESIDENCE OF THE PROPERTY
	1. 1.	
14250 1 1 1 1	15 10 CI W	
	The second of th	
: : : : : : : : : : : : : : : : : : : :		
		The second state of the second
		Commence with the control of the con

CASE FOR FLIGHT CASE WILL	•
STR as percent	
i	
SPECTON PASSON B FLEND AND STREET	
HISSIG: SPICETON :S S	
HISSIGN NO REPERSALINE MERCITA	
S TOTAL NO. WE PEAL OLL FEE	
18 RANDUM	
ALGOSIAN TIME DISTRIBUTED INTERVALS	
SAN NO VILLOUS LES NE MY PAGE	
1	

1 1
WISSILM NUMBER 1 WISSION TATERVAL NO WUMBERZITE INTERVAL NO MUMBERZITE
1 MISSION INTERVAL NO NUMPRAZITE INTERVAL NO 1
ANT NO NUMBERALIFE INTERVAL NO NUMBERLIFF INTERVAL NO NUMBERALIF
2 MISSION INTERVAL NO 1 NUMBERALIFE INTERVAL NO 1 NUMBERALIFE INTERVAL NO 3
HISSION INTERVAL NO Z NUMBERIALE
Ш

RUN 40 1 DATE 12/ 3/1973 PAGE NO 3
SIBSION NUMBER 1
lant-ope (ax) Marifining per filtent s &
SUPPLE OF INTERVALE IN MIRBIGH 4 3
MISSIN INTERVAL NO 1 MIERVAL NO PLT LUADS/FLT INTERVAL NO PLT LUADS/FLT
FIESTON INTERVAL NO 2 INTERVAL NO PLT LUADBOFIL INTERVAL NO FLT LOADBOFIL
DISSIDE ANTENNAL MI 3 TATERNAL MO FLT LOADS/PLT THIERVAL MO FLT LOADS/FLT TATERNAL MO FLT LOADS/FLT
LANDING TAXT MAXIMUMP PEM PLIGHT . 1
. •
השהעודן זאכרהסבס
STRESS AT REST IN TAME-UFF CUNFIGURATION B -19000.
TARE-OFF TAIL MAINUM TORD SPECTAUM
88316
ALTHER OF UCCURRENCE AT EACH STRESS
TARKAR TAR TARE
ייין אין אין אין אין אין אין אין אין אין
- 10000 ON THE PARTY OF THE PAR
ACTORES OF DICCIONENCE ALERCE ACTOR

On 35vd
C. I far annual
INTERVAL BURBER
04 (6.58)
25000. 2700s. Number of officer
FLIGHT MINIUM LOAD SPECTRUM
ווונצגיון וחשילה
\$14£33 \$000 700u
AU-MER DE OCCUMENCES AT EACH STRESS
THEREN NUMBER
7400.
YUMBER OF LICENSEMES OF EACH STRESS
PALGAT TEMPERATURE SPECTRUM
1
1 E 1 P 1 P 1 P 1 P 1 P 1 P 1 P 1 P 1 P
AND R OF ULCUMENTER OF ULCOURSET
O P P CALM TEMPERATURE

RUN FO 1 0ATE 12/ 3/1973 PASE NO 9
A PASSAGE A
/
PLIGHT MAILWAY LOAD APRETRUM
31468 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
KANTER FRANCE AT EACH STREES
•
FLIGHT WINIMUM LOAD SPECTRUM
INTERNAL ANNER 2
(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)
ASPO. TAPO. AND UCCURRENCES AT EACH STRESS
7 7
FLIGHT N.E G. LOLD SPECTRUM
INTERVAL NUMBER 2
1186
MONOWAN THOUSAND THE STATEMENT STATE
FLIGHT TEPERATURE SPECTHUM
2 1970-0-1 1-A831-1
「一日の一日の一日の日の日の日の日の日の日の日の日の日の日の日の日の日の日の日の
207
PACKER OF OCCUPENERS AT EACH TEMPERATURE

0 362	
TRUCK-AND-GO Allitur Transe	
THE THE PARTY IN THE PARTY WITH	
049.00	
1381	
TOTAL OF MICHAEL STREET	
TOUGHER DE COLLEGE ONE 6 SPECTRUM	
23217	
0000	
WITHER OF OCCUMENCES AT FACH STORES	
TANDING THE STATE OF THE STATE	
AUR JAN STREET	
58318	
19600 A. Minhs & Co. Crimber Co.	
Z COUNTY COUNTY OF THE BOARD	
LANDING TAXI MAXINUM LUAD SPECIALIN	
9,888	
NO BEE OF UCCUMPLACES AT EACH STREET	
MARIA TELEVISION TO THE TOTAL TOTAL TOTAL TELEVISION TO THE TELEVISION THE TELEVISION TO THE TELEVISION THE TELEVISION TO THE TELEVISION TO THE TELEVISION THE TELEVISION TO THE TELEVISION THE TELEVISION THE TELEVISION THE TELEVISION THE TELEVISION THE TELEVISION T	
614818	
*112000 -11000 -11000 -11000	
NUMBER OF GGUNBERGE AT EACH STRESS	
e Juni 1 days come	
- 1	

AND TRANSPORTER AND	
Ι.	
- 1	
	ζ-
Ш	
MISSION INTERVAL NO 2	
TIZZEGENE SENE MINES	
Pilitin To Tay Pilet B	
THE PER PLANT STATES OF THE PLANT BE STATES	
PROPELL VOT INCIUDED	
STRESS AT REST IN TAKE-THE CONFIGURATION E	
1 1	
(1465s.	
-000010000000	
ACTUREN (IN DECUMENCES AT EACH STRESS	
TABEOUF TAKE MINEUM-LOAD SPECTRUM	
F P R E S S	
-7005 1000 1200	
TO TOWN THE WEST AT THE STATE OF THE STATE O	

On Shard State 212, 211 on white	ı
2 #3847F NDIG014	ı
	1 1
FLIGHT WALKUM LOOD SPECTRUM	
\$78k\$	1
Social Structures at Each States	1 1
PLICHT PINITUM LUAD APECIOUM	1 :
TATCHVAL NUMBER 1	1
TATE OF THE PROPERTY OF THE PR	1.1
JUNGER OF OCCURRENCES AT CACH STRESS	1.1
bilds ONE Glass APPENDIN	<u> </u>
Mile Right, Nutrite R	! :
37783	
MUNEER OF UCCURRENCES AT EACH STREES	1 1
	1
	1
	;
	!
	,
	,
	<u>.</u>
	1
	,
	,
	! !
	ı
	,
	l I
	1
	ı
	1 1
	i
	1 1
	- -
	1
10 Table 10	ı ı

N. STATE

MUN NO 1 DATE 12/ 3/16/15 PAGE NO 10	,
A NEW YORK WASHER A	
	1 1
FUELT MINISTER COLD SPECIALITY	
11/16/15	
ALVERA NO CELEBRATES AT EACH STREET	
F. L. C. P. W. W. L. L. S. P. L. C.	
AVENUE NUMBER	
\$ 9.5 mg	
19000	
NUMBER OF UCCURENCES AT EACH STRESS	
HARD STORE SPECTAGE	
2 #3400 1443149	
574155	
2000	
AUTHOR OF THE FACE BINESS	
	,

C PERROP HIMRE 2
TOLERANDED LANDING THARFT (DAD APPETSHIE
= 1 1 1 2 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
ALPHER IN COCCUMENCER AT EACH STREES
INKHAND-60 LANDING ONE G SPECTRUM
A 70 B. A A A B. A A B. A B. A A B.
ALIMPED OF UCCUMPENESS AT EACH STRESS
LANDIAL PREST LIAD SPECTALIA
-1740A -1740A
ALTER OF HECUREACES AT EACH STRESS
LANGING TANT WANTHUM LING SPECTPUM
CORP
ALTER OF UCCLARACTE AT MACH STATES
,
TANDER TANE MINE TOLD BORNING
1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
STREET OF USE OF STREET
SHUDED CONDITION TERRESTATION SO.

TANAMAN AND THE PROPERTY OF TH	TENY LOSE ABO		OH JOHA) I				
PLIGHT NUMBE		יבייניים יומים שנפטפאל	COURNE					
BEAT VOINGE	LOADS . SB							
LOAD NUMBER	STHESS		LUAD NUMBER	DTHESS	TENP	LOAD AUMBER	4.40.64	46.24
	-2000	500	~	-2000	39.		-6000	500
	*000v	30.	-	2000		4	-4000-	29.
	2000	200	=	-0009-	30.		25000	299.
9	25,000	570	-	25000	270.	51	7900	250
	7900	250	200	27000	250,	10	27000,	270,
77	CAOOD.	240	2	12000	240	17	6000	279.
	11000	260.	2	26000	260.		70000	200
	64040	2000	2	90059	260.	01	28000	200
	28000	6000	~	20000	260.	?	10000	240
- 47	100	78.6		12000	200	•	31000.	275.
0	29000	275		20202	265	2	-	275.
5,	6700.	3.5		70070	25.	42	11000.	205.
97	31000.	266		2000	6734	45		255,
6.0	0700	275		100/4	265	3	31000.	255,
25	15306	100		27.200	200	3		50.
53	-0100		2 2	2000	3	2	-11000	20
95	112000			None in	24.6	22	-6400	50.
			2	7,1	0	00	9	
								!

	0416 12/ 3/1073	PAGE NO 13				
3	LUAD AND TEMPERATURE BEQUENCE					
S STATES STATES						
LUAU SIPPRES	TENP LOAD NUMBER	LINGER STREES	94.97	DAD SOLUTION	, , , ,	
1 -12050			59.	A	-12080	18.N
7 -7009.	59.	A -7000	28,		-0000-	30.
20005	30.	11 620	59.		2000	28.
10000		19 32000	59.	57	10200	50.
1000 a 61	50.	20000	838		26000	65
- \$2 K0009.	765	7000	29.		0000	50.
2000		20 - 1 9500	50		6700.	50.4
906.1	200	6700	59,		-17000	59.
34 -10200	50.	36 -10000	265	12	-7190	59,
100.				2	-102001	50,
40 -10000	59.	6700	265.	20	2000	59,
						1221

						·

NUN NO 1	3140	6416 12/ 3/10/3	PAG	PAGE NO 14					
CIGHT-NITCH	1040 AND	THE THE PERFERENCE APOLICE	١L						
THE PROPERTY OF THE PROPERTY O									
# 80401 43 #38108	_								
848 BAB-D- G9GT	. 53	THE GAD AUMENT	NUMBER !	494640	4:46				
bute	900	200	~	-5000	50.	TOYOU WOMEN	914666	rene	
	000	500	٥.	-1000	50,	•	2000	33	
S	0.0	105	=	0000	700	•	-0000	5.5	
25/2	200	501	=	25000	270.		27000	254	
1200	00	.00	_	7400	250	-	2000	250,	1
25 2400	5	90	22	25000	260	12	6500	200	
26 26	200	0.0	2	. 6000	260.	7	26910	200,	
11 500	100	100	2	7000	255,	0.00	2000	2002	
265	100	95.	2	31000	265,	3	7600	100	
37 670	.00	55.			2051	3.6	31000.	75.5	1
0041- 0*	3.	.05	1	10001	300	30	0000	50.	
0948	0.0	0.00		112000		2,	-11000	59.	-
00007110	10.	50,		6700.	246		-6700	59,	
					1203	•	310000	.455	1
									1
									i
				}					l
									1
									1
									1
									l
									ί.
				1					
									l
									l
									į
									1
									l
									l
									!
									1
									I
									l
									1
									ł
									l
									l
									1
									1
									((
									1
									1
									1
									1

E DN NIN	DATE 12/ 3/1973	3 PAGE NO 15				
	FLICHT LUAD AND TEMPERATURE REQUENCE	BEQUENCE				
S S S S S S S S S S S S S S S S S S S						
SCHAPES SHAPES	TEMP	LUAD NUMBER STREET	164.0	LOAD MINNED	010568	8 M 3 4
1			265		-12000	59.
	29.	5 -12000.	59.	9	-8000	505
100011 01	200	0000-		•	-12000	59.
1	20.	14 20000	205	2	4400	240
*	5	17 4800	59.		24000.	50.
10040	!	200585 05	20.	7	9819	59.
25 -14500	594	23 6800	29,	**	-185004	50.
ï	0,0	26 -17000.	591	27	-7400	59.
7,0401. 97	88	į	59.	30	-10600.	201
100201- 11	59.	35 -10200	59.	33	-10200	50.
	-					
		The state of the s				

LOAD NUMBER STRESS TENP 3 1200. 59. 4 2000. 59. 15 2000. 59. 16 2000. 59. 20 10500. 59. 20 10500. 59. 20 10500. 59. 20 10500. 59. 20 10500. 59. 21 10500. 59.	
1000 NUMBER STRESS TEMP STRESS	
Table 1	

Pur ng Dall 12/ 1/1973	- 1			
1 1 1	27			
ALVARE OF LORDS - 60				
AND MINASES STREET				
- 12600 NUMBER	$\ $	LOAD MINES		
=	1969	29.	* 9000	- F. F.
20000		200	-0000	59.
	2000	59.	50000	335
	8000	100	1	
4400 Ses Ses	4400			50,
7400	6700	27	1	9.6
~ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	200	30		30
10 -10/20		59.	10500	786
	-6709-	94	-7100.	59.
		9	-11600	59.
				!

As noted in the introduction, the spectrum printout as given by this routine may not be useful for subsequent use in fatigue or fracture mechanics calculation. It should not be difficult, however, to modify this program to form the desired linkage through magnetic tape or other device.

IV REFERENCES

1. Lincoln, John W., ASD-TR-80-5037, <u>Development of an Aircraft Maneuver Load Spectrum Based on VGH Data</u>, July 1980.

APPENDIX - SPECF PROGRAM LISTING

This listing given below is a FORTRAN extended language routine. The DIMENSION statements are set up for an aircraft flying twelve missions with ten mission intervals each. The EQUIVALENCE statements are compatible with a spectrum for fifteen missions with eight mission intervals in each mission. Consequently, this case may be analyzed with a simple DIMENSION statement change.

PROGRAM SPECE (INPUT, OUTPOIL) TAPES BIRPUT TAPES BOUT PUT)	
FOR A PATISON TROPT PATISON TO SECUENCE	
CONTRA P(13000) N(13500)	Γ.
2072 CON 174 CON 177 C	
91	
	٠

With Little And Annual Control

Paritiment - Parit	TAPUT 74/94 OPTS.	7N 9,64P153 62/01/79 17,37,82, Pige 1
	C BURNUTINE FOR EMPUJ UF PLOATING AND FIRED POINT NUNBERS	OINT NUMBERS OF IN 2
	INTEGER DAY, YEAR EQUIVALENCE (N(1)	NPF13, UEIN A
	((N(3), NPF2), (N(4), NPF3), (N(5), NP	50 NI 30
		, NA),
10	2 (1(13), KABS), (H(1A), H(SEPT), (H(10), HUNE	6), (N(16), NF(T), DEIN 46 6) DEIN 49
		6 N 2 10
51	C N(2) B NPF1 - NUNGER 17 SETS OF PARAMETERS TO BE READ	O DE READ USTA O
		D BY FORMAY 2 DEIN 10
	TO THE POST OF THE	BE READ BY DEIN 11
92	TOTAL B NOTE OF STANFORD STANFORD OF STANFORD ST	BY PORMA 4 DEIN 13
	C Learner of the control of the cont	131 VIST
	C NOTE TO STANK OF INTEGER PROATE TO BE NEAD	AEAD AE OFIN
52	THE CONTRACTOR OF THE CONTRACT	D N 130
	W(10) B VEAR	91 *130
	TORE ATTORNOON OF THE STATE OF STATES	MECHANDO DATA DEIN 17 MISSION PROFILES DEIN 18
30	C N(12) B N4 - NICARRY OF MISSIONS AND GANDON V SE	DEIN 19
		NPANDOM DEIN 21
	THE TANK A PROPERTY OF THE PRO	(CASE 1) 0E N 23
33	C A(12) R PERS B BUILDER OF TIERS B NONSENDOR	THE FOLKS OF THE STATE OF THE S
	SETUENCE 18 REPLATED IN UNE LIPETING	061h 27
	NONSANDER DECUEACE	PELECTIONS IN A DEIN 20
67	TALKON I PARET TARABLE TARABLE TO FORTA	05.1% 30
	1 (101) a SP(1)	28 ×130
	C P(415) # 8174(1,1) 5	\$5 X130
50	2 P(715) = SPP(1,1,1)	OF IT
	6 P(5515) # 8F6(1,1,1)	95 M 37
	C P(7915) = SLT((1.1)	OF IN SO
95	C P(8515) # 8 [M(1,1) 5	00 M 30
	C P(1215) a P((12121) 5	15 Kl 41
	P(11515) = 8166(1.1)	0 (N 43
55	C NOT DATA - INTEGERS - INPUT FORMAT	DE IN 68
	C W(815) 8 MTW(1,1)	DEIN 46
	C N(715) B NFP(1,1,1) 6	DEIN 47

	9674 40
	06 14 40
	05.14 St
	DEIN 52
	0£1× 55
	0E1% 54
	0512 SA
	DE 12 54
	ACTU 62
	V. L. 21
	20 M 20
N(12005) = M(121) 10 10 10 10 10 10 10	65 NI 36
	06 KI 30
M(1222)	DEIN AL
	29 × 190
	2 E E
	15 12 A4
	06 Th. 46
N(12355) = N(10(1) 3 1 1 1 1 1 1 1 1 1	70 TM 02
N(16200) = h(1) S N(1620) N(16200)	DE IN 90
	061% 67
	DE IN 68
	AFTR 40
	A 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
((1290n)	DETM IN
# # # # # # # # # # # # # # # # # # #	05 IN 71
	DEIN 72
### ### ##############################	DEIN 73
16 (1205) a NEAC (1.12) 6 16 (1205) a NEAC (1.12) 6 16 (1205) a NUML (1) 17 (1205) a NUML (1) 18 (1205) a	06 th 74
20 10 10 10 10 10 10 10	06 3 V
20 13.75 19.75 1	
20 FUNNAT (347) 20 FUNNAT (457)	
10 FUNTAL (1941) 10 FUNTAL (1941) 2	UP.1% 76
20 FUNNAT (141)	06 × 30
16 FUNDAT (141) 20 FUNDAT (141) 20 FUNDAT (141) 21 AND	DE12 80
20 FEAR TABLES TO SEA T	06 TK A1
20 FURNAT (344) 20 FURNAT (344) 20 FURNAT (344) 20 FURNAT (315) 20 FURNAT (415)	06 (1 42
20 FUNDA 1 136N 1 1 20N 2 1 20N 2 1 30N 3 1 30N 8 EAD IN PAR 10 FURNAT (6E 1 10 PEAD IN PAR 10 PEAD IN	76.17.06
20 FURNAT (20) 1 A 304 2 A 304 2 A 304 2 A 304 2 A 304 3 A 3	UE1 02
2	95 M 30
20 FUNNAT (1967) 2 A 1964 3 A 1964 30 FUNNAT (1115) 10 PEAD IN PAR	OE 12 95
2	06 IN 66
2 / 35 / 35 / 35 / 35 / 35 / 35 / 35 / 3	DEIN A7
20	AC 14. AA
10	70.00
10	UCJW 69
10 FURNAT (415) 10 FURNAT (415) 10 PEAD IN PAR 10 PEAD IN PAR 10 PEAD IN PAR 10	DE 14 90
10 FORMAT (119 10 FORMAT (119 10 PEAD IN PA	CEIN OI
20 FURNAT (313 20 FURNAT (413 20 PEAR 1 (421 20 PEAR 1 (421 20 PEAR 1 PAR	05 fk @2
10 FGPAT (118 10 FGPAT (118 10 PEAD IN PA 10 PEAD IN PA 10 PA	ACT 1. A.
10 FURNAT (115 10 FURNAT (661 10 PEAD IN PAR 10 DEAD IN PAR 10 DEAD IN PAR	
10 FURNAT (OE 1 P P P P P P P P P P P P P P P P P P	N 128
20 FUERAT (OE) 10 PEAD IN PAR 10 D	VE IN 95
10 PESD IN PAR 10 BESD IN PAR 10 B	DEIN GE
20 22	76 11 04
2 2 2	AS IL OR
2 2	- VEA - ZE
29	
110 60 DO 100 J 4 14 MPE2	DE 14100
LEAD (A. CO.)	DEIN101
	DEINIOZ
TO THE TAX ATTRIBUTE OF	DEIN103
	26 72 04
	25. 1. 1. 5. 5.
C READ IN INTEGRES OF FURNAL S	25.4% 02

SIBRUUTENE TAPUT 74774 OPTEE	e1 Ftw 4,0+2353	02/01/74 19,39,222, PAGE S
115	(MPF3) 120, 160	90 IN130
120	150 1 o 1, NPF3	DE JW107
	CALLOS ANGLIS ANGRES ANGLES	00 1 1 1 0 0
130 FURNAT (SI	25 AD (5, 540) (N/3). J B NNG11, NNG22, NNG33)	0614110
140 FURNAT (12	1	0614111
150	30.51	-
1931-11 NI OV 3M	THE BALL AND THE PROPERTY OF T	0F.IN.115
	200 101 101	# 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2
774	(5, 180) T. M(T)	05 Pulls
11 .27 141614 000	(5)	DE1N17
190		DE1X110
TAVANT IN PARAME	TENS BY FURNAT S	UE 14119
002	(hPFS) 210, 240	0F14120
150	230 I m f 2013	0514121
	B 300 (F 23 (C) (DE LAIRE
1	75 25 25 2 25 25 25 25 25 25 25 25 25 25	No twice
220 608mAT (715)	1276501 21	DEINISS
	E	0E [4] 26
1	1), 15 e 1, N3)	UE 11127
230		DF14128
C READ IN TRIEGE	HE BY FURNA! 6	DE IN129
540	(NPF6) 250, 270	UE 1N130
0.3 05% 001	200 1 m 1, APF6	0£ IN131
UA 38	1 (5,220) N6SETS	DE (11) 32
02	COO TELL SOREIO	20 LW LS 20
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	25 5 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
		4F - V - 4G
200	I WILL	DE [N137
270 CALL	INAID	DE14138
0.38	281	DE 14139
6N3		UE IN140

	C SUBROUTINE FOR MRITING THE INPUT DATA C CULPUM PILSSOD), MILSSOD)	TAO M
3	1 SFF([2,10,20], SFM([2,10,20], SFF([2,10,20], SFM([2,20], SFM([2,	NAD 5 NAD 6 NAD 7 NAD 0
10		NAD 9 NAD 10 NAD 11
81	1 NIF(12), MIN(12), WFP(12,10), WFW(12,10), MFG(12,10), 4 NII(12), MIP(12), WILN(12), WF(12,10), MIG(12), WIG(12), 5 NS(12), NIK(12), WIEMP(12), WIF(12), MFF(12,12,10), WIF(12), 6 NAUD(15), MUNHP(15), WFMC(13,12,10), WUHL(12)	NAP 12 NAD 18 NAD 18 NAD 18
	1 (0(415) 5110) (0(15) 19) (0(15) 810) (0(15) 1 810) (0(15	NAD 18 NAD 17 NAD 18
50	2 (P(7945) 9L1), (P(P215) 9LP), (P(P315) PLTM 3 (P(BA15), (P(1) (P(1) 15) G(1), (P(1) 15) 9TG FOULABLENCE (M(1), (P(1) 1, (M(2), MPT	NAO 20 NAO 20 NAO 21
	1 (0.63), MPP2), (M(43), MPP3), (M(5), MPR3), 2 (M(6), MPP3), (M(7), MPP3), (M(10), YEAN) 3 (M(8), MPP3), (M(40), DAY), (M(10), YEAN)	NAD 22 NAD 221 NAD 23
\$2	1 (A(13), MARMA), (M(15), MCASS), (W(12), MM), (M(10), MF, 17), (M(15), MM), (M(10), MS, 17), (M(10), MS, 17	NAD 24 NAD 24 NAD 24
	Editaliantene (Atta), Mith), (Mess), MINS.	NAO 27
90	2 (*(715) *(145) *(*(315))	NAD 30 NAD 31
35	6 (11(23) 11(1) (14(1225) 11(1) (10(1225) 10(1) (10(1225) 10(1) (14(1225) 10(1	440 33 440 33 140 34
	4	NAO 35 NAO 36 NAO 37
0.	2 (N.(12055), MAUM), (M.(12065), MUMMPT), (N. (12065), MUMMPT), (N	NAD 36 NAD 40 NAD 40 NAD 40
3	20 FURMAT (/10X, 45H	IND GE
		14.0 45.
95	SO FUNNAT (/10x, 1745PECTRUM 6ASE	NAD 47 NAD 48 NAD 49
	3	15 Over 05 Ove
55	$\Pi\Pi$	14.0 5.1 14.0 5.4 14.0 5.4

500 TAS 120 TAS 120 TAS 120 TAS 1	INAD SO
GG 70 156 WRITE (6.120) HNUHS, HISRPT	INAO SE INAO SE
TORANT (/10%, JOHNISSION SELECTION IS NOWANDOW 1 710%, SANNUNGER OF DIFFERENT HISSIONS IN	INAD 60 INAD 61 INAD 63
(3)	INAD 63
FORMAT (710X, MAH.	IXAD 66
135 REITE (6,140) I, HUMRPY(1), T+1, HNUM(1), HUMRPY(1), T+1, HNUM(1+1), T0 HUMRPY(1), T+2, HNUM(1+2), NUMRPY(1+2), T+3, HRUM(1+3), T-1, HNUM(1+2), HNUM(1	INTO 67
FORMAY (115, 215, 119	INED YOUR THE YOUR
FORMAT (/10x, 22HHISSION I	INAD 72
77	INAD 74
TAIL VIERA	INAD 76
BO 140 I B 1, NM	INAD 82
181 8 V6(1)	INAD 83
HPITE (INAD 632
180 FUREN (10x BHRUSSON NUMBER, 15, 2x, 3x, 3x, 3x, 3x, 3x, 3x, 3x, 3x, 3x, 3	INAD BAS
1.9) BLICA	2
E L	INAD BUY
S AX, LIMONBERALITE)	INAD BAS
X + X = ZdX	
190 KP1 B K + 1 KPKAC(KP1,J), KP1, WPKAC(KP1,J),	INAD BAS
I MPZ, NFRACIKPZ, I	INAD GGA
501 101 1121 2123	-
ZIO NATAE (6,220) ZIO TORNAT (10X, 25HMIASION TIME IS NORMANOUN)	INAD 69
C MAITE OUT MISSION LOAD AND TE	INAD 91
100 C23 DO 390 I # 1, NF	INAD 93
CALL OAG	INAD 94
اد	96 QVNI
	INAD 97
740 FORMAY (7)04, SSHIRKE-OFF TAXI HAXIMUMS PER FLIGHY E, 15)	INAD 99
CENT TO ROUGHT AT STRACTURE CORRES TO STORY TOWN TO ROUGHT TO STORY TO STORY TOWN TOWN TO STORY TOWN TOWN TO STORY TOWN TOWN TO STORY TOWN TOWN TO STORY TOWN TOWN TOWN TOWN TOWN TOWN TOWN TOWN	17 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
NSI B NS(I)	INADIOS
18 1 = 1 00 200 00 ER	150104VI
Z60 FURHIT (/JOX, TOHMISSION INTERVAL NG, 15)	WAD1053
1	

	}	I WANTERVAL	NU. 2X. 13MFL	FLT LOADS/FLT. 6X	SAC SAMPLY LOADS/PLT. AND SIMPLEMENT NO. SEC.	INADIOSA	
	~	134617 104067	15			1 WAD 1 05	57
			3 0 K	1, WHT40, 3		NAD106	-
1.56		202				TAN LOS OF	100
	270	1	RHITE (6,280) K,	K, MFF (K, 1, J), K	AFF (K. 1. J.) API NFF (KPI. 1. L.) .	INADIOS	99
	-	KP2, NFF (AP2. I	(6,1)			INAD1665	65
1	200	FUPMAT (T21,	5115)	N. VET IV		OF CANAL	
136	26.0	FLRNAT (/10)	WICKA IMAK	G TAXT MARINUMS P	E FLIGHT 8. 753		
			176 (6.500)	NTG(I)		NAD11	~
	200	FURNAT (/10)	S CANNUMBER	FURHAT (/10x, eahhumber OF TOUCH-AND-60 LANDINGS PER PLE	TOUCH-AND-60 LANDINGS PER PLIGHT C.		
	-	15)	40 / 110 11	110 110 100 100 100 100 100 100 100 100		210441	
110	937					STORN	
	150	FURNAT (/10x.	, •	SHIEMPERATURE PROFILE NOT INCLUDED	INCLUDED	OL TOWN	
	•)9	2			INADI	1
	3.50		#RITE (6.540)	:		STIONAL I	
	340	FURNAT (/16)	L ZenTfribER	ATURE PRUFILE INC.	FURNAT (/10x, Jentendenature PRUFILE INCLUDED)	14011	0
145	320		116 (0, 564)	() X		NAD 22	
1 1 1 1	000	PORMAT (/10x	IN BONDIKESS	AT HEST IN TAKE	DEF CONFIGURATION BY	JAADIZ	
	-	11000	1067 (4) 1901			S TO THE	
	1.70	E.10447 (4110)		CALL TONIANGE TAXI MANTHEM I DAD BOSE TONIA	DAN BOSPPOIN	2	-
444	-	× 0 × 0 × 0 × 0 × 0 × 0 × 0 × 0 × 0 × 0	65 401 5114			CIONI	
		*	12	Į.		INADIA	
	-	•	WATTE (6, 380) ((STIP(I,J), J = 1, MITPI)	1, MTPI)	MADIZ	4
	380	FURNAT (16F11.0)	1.03			INADIZ	
		×	116 (6, 590)			LINADIA	•
145	390	FLIRFAY (10)	SONWINBER	FURTAL C. 101. JOHNUMBER OF UCCURRENCES AT EACH STRESS	T EACH STRESS)	INAD130	01
		2	11E (6,400)	(NT1P(1,1), J e.	1, HTPI)	INADIS	
	000	FUPHAT (10111)				INADISA	
			= '	(0.410)		TOWN	
125	-	ADMINI LA	1	LOUISIL THE	UND STEEL HOR	1	
126	-	200			***************************************		
			7002	A CESTULIA COLO		1041	
			TF (6. 190)	(0.100)	,	NA P	
		2	(11E (6,400)	(NTIN(T.J). J B 1. MITHI	I. MINIT	INAD139	0.1
155		3	PALE . NPAGE			INADIGO	9
		3	IL PAGEND			INADIA	11
		1	(116 (6.230)			INTOTAL	11
		Õ	200	18N,		LANDIGE	
	4.44	01 317 84	7777	200	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	200	
100	2	01/1	THE MANUAL PROPERTY	PRINCIPLE TARACTURE OF STREET		STIGANI	9
	1		AMB TAF SE			INADIAL	9
	•	1	Contract of the	(6)		INAMIA	
		-	1776 (0,300) (8	(BEP(Leden), N B 1, MFPLJ)	1, MFPLJ)	INABJAB	91
165		ì	1116 (6, 390)			IMADLES	6
			HH 116 (0,400)	(e, 400) (NFP(IsJeR), R m 1, MFPIJ)	11 MEPAJ)	STOVAT	9
		ı	(116 (0.430)	7		INADIS	1
	430	FURNAT (716)	1 20 WELL GH	CLIOX, PONFLIGHT MINIMUM LUAD SPECTRUM	CIRUM	INADISZ	2
	1	710	15m1 m1 m	AL MUMBER 15		I TADI S	2:
	1	170 TV				STANT OF	
		•	(7,1)245 8 71745	(7,			2

13	PUBLICATION IN THE PROPERTY IN	INAID 74/76	0PTs) FTW 4.44P393	02/01/74 17457.20. PAGE 4
### ##################################			[15 (a. 180) (afternament & a. a section	1440154
## 17 (2011 19 19 19 19 19 19 19 1		184	11E (0,390)	1440157
440 FURMAT (LIGHT CARE & LOAD BYCTRUM 1041 194			(86848)	1440158
	1.5		(9,440)	\$410159
		7 184401	1SHINIENVA	LAPIDE I
## 10 10 10 10 10 10 10 10		// 2	9H84B	1~40162
		13 da 2	GL1 B MFGCT.J)	INADIOS
\$50 FGRMAT ((1)01 (1)00) [W.F.G.L.J.L.] & R.E.T.WUM \$50 FGRMAT ((1)01 (A01	3 3	11E (01580) (SFG(12JAK)2 K B 12 HFGLJ)	INAC (64
### 100 (177 1977 1		23	TTE (6.400) (NFE(1.1.K), A S 1. NFE(1)	1940166
10 10 10 10 10 10 10 10			TO (475,450), NTEMP(1)	[HAD167
20		920	7 (047.4)	64107K]
## 12	102		CATALOGICAL TEMPERATURE BESTANDA	641042
## ## ## ## ## ## ## ## ## ## ## ## ##		2 //101/	LATA STRUCTURE S	0.404KT
#### (** 340) (** (** 1. ** 1.		1 4 4	() # MF(1,0)	NA0172
470 FORFAT (107, 41 MINERS (10 DECEMBENCES AT EACH TERPERATURE) 100, 400 400 400 400 400 401 401 401 401 401		¥	17E (0.180) (7F(1, J, K), R B 12 MF1J)	1×40173
475 475 476 477 477 477 477 477 477 477 477 477	921		11F (b, 470)	
475 480 480 480 480 480 480 481 480 480 480 480 480 480 480 480 480 480		470	THE STATE OF COCCEPENCES AT EACH TENESTICATE	
\$10 FORMAT (/10*) 1 FORMAT (/1			Classon field for the property of the contract	TANDANE TO THE PROPERTY OF THE
\$10			166 B NPAGE 0 1	47.04.74
\$10	561	CAL	L PAGEND	1840170
\$10		104	116 (6,230) 1	[NAD179]
Park Color		\$00	-T1WUE	[wan] 80
10 10 10 10 10 10 10 10		V d d	Lof a MPAGE + 1	1%AD181
\$10	900	CAL	11 PEGEST	12401AZ
520 FURNAT (1721 ANTOCHAMO-GO LANDING THEAST LOAG SPECTRUM TANDING THE SECTION (1721) 1 (1721 ANTOCHAMO-GO LANDING THEAST) 1 (1722 ANTOCHAMO-GO LANDING THEAST) 1 (1723 ANTOCHAMO-GO LANDING THEAST) 1 (1724 ANTOCHAMO-GO LANDING THEAST)	- FVV	7 9 b	112 100634 1	14401621
10 10 10 10 10 10 10 10		510	(6.520	
1 // (1) (525 FURNAT (/10	THIDUC	
## ## ## ## ## ## ## ## ## ## ## ## ##		1,0177 1	010100	
## 11	205	9.1	31	CO.CAST
5.20 FORMAL (//01, 1) SHIPE (12,7), J. B. 1, MIEEZ) 1		₩ 13 13 13 14 15 15 15 15 15 15 15 15 15 15 15 15 15	TE (6.300) (9761(1.3), 3 a 1, M0111	INAQ100
		23	(0.5.4)	DO CVA
\$10 FGRAI (/10;)SHINGTHANDING (AND THE ONE E BPECTRUM WIND W			TE CALLED MINISTER J. J. 12 MISSES	OOTOWN
1 ((101) 04514631 110 (101) 04514631 111 (101) 04106 (101) 1. J. B. J. MIGGZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZ	210	5.10	SSHIDUCH-AND-GO LANDING ONE & BPECTRUM	1740102
		1/101/	CECATE COD	\$ 610 V
		9	1991 1991.	INADION
348		2 3	16 (6.200) 18156(1.2). J. B. J. MISSI.	50 C C C C C C C C C C C C C C C C C C C
\$40	215	**	TE (0,400) (NTGG(1,3), J m 1, MTGG1)	TOAD 197
230 FLEMAN (1/2012 SENEANDING INPACT LOAD SPECIALM 1 (1/2012 - MISTERSO) (MISTERSO) (MI		946	16 (6,550)	INADIOS
		539 F LM# 4 T	Samlanding Intact LOAD SPECIALM	Inap199
##ITE (0.180) (815(1,1)). J. B. 1. W.11) ##ITE (0.180) ##ITE (0.180) (815(1,1). J. B. 1. W.11) ##ITE (0.180) (815(1,1). J. B. 1. W.11) ##ITE (0.180) (815(1,1). J. B. 1. W.11) ##ITE (0.180) (817(1,1). J. B. 1. M.17)		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	O'LALIN O'LA	INAUZOO
##[[[(0.198) Chif(1,1)	224	100	TE (4.160) (SLECTAL). J. B. 3. W.11)	TAROSO.
		1 2 X	16 (64,190)	140203
SAG FURNAT (2.18%) ANY AND MARINUM LOAD BPECTRUM 1440 1 (1.18%) ANY AND MARINUM 1440 1 (1.18%) AND MARINE (4.18%) (4.18%) AND MARINE (4.18%) (4.18%) AND MARINE (4.18%) (4.18%)		2.3	TE (6,400) (611(1,1), J = 1, ML11)	1440204
1 //10% - 0+0/106.55)		640	1	JMAQ205
MITE (6.392) (SLYCITAL). J B 10 MITET) Edite (6.392)	226	-		1w4020b
WEITE (4.390) (ALTOSTALL). J. D. 14. HLTPI).			757 # 21 POSES	7.6704×1
bb11£ (4.19g)		122	18 (6.380) (8.70(T.3), J # 1. N.797)	LARGE GALL
		[84	16 (6, 190)	TAA0210

27,20c PAGE S					
62/61/74 17,37,26.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				
BURROUT INC. That D - 24/24 OP fai - 57 4 4.000 151	\$10 \$70 \$70 \$70 \$70 \$70 \$70 \$70 \$70 \$70 \$7				

SUBMOUTER COM	70/70 OPTO1 OPTO1	02/01/74 17.37.334 PAGE 1
	BLALDUT ING CORE	
	STING COMPATIBILITY OF INPUT DATA	Chip 2
	ij	COMP 3
	OINTMETCH MITPLIZZZO1, MYTM(12,201, MFP(12,10,201,	
	1	2 740
	THE FALL COLD TO THE TABLE TO T	6 Aurija
1	THE PARTY OF THE P	
	CALLAN ATEMPTICAL CONTRACTOR AND CALLAND CONTRACTOR CON	
	TAILED TO THE TA	
	THE TAX TO	
	一つのでは、「「はなった」」では、「なった」、「なった。」、「なったった。」、「なった。」、「なった。」、「なった。」、「なった。」、「なった。」、「なった。」、「なった。」、「なった。」、「なった。」、「なった。」、「なったった。」、「なった。」、「なった。」、「なったった。」、「なった。」、「なった。」、「なった。」、「なったった。」、「なった。」、「なった。」、「なった。」、「なったった。」、「なった。」、「なった。」、「なった。」、「なったっ	COMB 12
	PRINCE Trutter Traine (Title) Trible	TOTAL DESIGNATION OF THE PERSON OF THE PERSO
	TANKS AND THE PROPERTY OF THE PARTY OF THE P	
	THE CONTRACT OF THE PROPERTY OF THE CONTRACT O	
	アイ・マー・アイ・アイ・アイ・アイ・アイ・アイ・アイ・アイ・アイ・アイ・アイ・アイ・アイ・	
	12 12 12 12 12 12 12 12 12 12 12 12 12 1	
	12121 - 11212 - 11212 - 11212 - 11212 - 11212 - 11212 - 11212 - 11212 - 11212 - 11212 - 11212 - 11212 - 11212	
	Tribut of the state of the stat	
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 A 1 A 2 A 2 A 2 A 2 A 2 A 2 A 2 A 2 A
	(1.62221	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	764 //645/1 //645/11	10 T
	COLUMN COLUMN AND AND AND AND AND AND AND AND AND AN	22 440
		0.40
· · · · · · · · · · · · · · · · ·	WUT (N(12995), BUNTPLD, CA	72 AHO
	(×(1)25-0-7) NOTE:	\$2 avos
		92 4403
	NA 1 8 1 840	COMP 27
	CIECK ON NORMER OF TARFORF TAX MAXIMUMS IN ONE LITERINE	92 4WD3
	HITPL B HITP(I)	S. A.E.
27	NICAL B PUMP (I) A ATTROL	SCORP 30
	MCME & C	77 4403
	01: 10 1 m 1. MTPE	32
-	PERK B STIPETLOD + NCHK	10AP 33
	IF (NIEST - MCMK) 200 40	Sec. Sec.
9	MRIJE (04.30) IL NTEST, NEN	COMP 35
2		CORP 36
	TOWN TOWN NO. 151 - 2x, Trivited to 121 - 215 - 61MCHA H. 150	COMP 37
	MCONT B 1	0. a.v.
	CITCH ON MUSEUM OF TAKE STREETING IN ONE LITERATURE	05 de 20
96	CIVILLE B INTER	07 4×03
	0 B VZZZ	0.49
43	THE TOTAL OF THE STATE OF THE S	29 4403
	CEST - CONTROL E ELLE	
	2	97 G10
	ACCESA CAN AND ACCES OF THE CAN ACCES OF	
-	MANAGER AND TALL THE SERVE OF	
		4 6 MC
	CAMPUS CA ALLEGED CA NO. COLO MANAGEM BOCK - COMPOSED	
		CORD 6A
	LEX - 4 CC	CO20
	A STATE OF THE PROPERTY OF THE	COMP 52
A8		
	AND THE RESERVE	
72	ETTER B EFFECT. 1.37 & EFFECT. 1.17 A EFFECT	COMP GA
	ee ca in	COMB 63

BUSHOOT INE TONF 74/74 CHTAIL	82/61794 17.37.35. P.68E Z
The same of the same of	
100 000 000 000 000	COMP 50
DO 118 0 1. MPT	2.2
110 SCRE B SPECIAL ON P SCRE	ON THE PARTY OF TH
IF (NTEST - NEWS) 120, 140	2 000
- 1	04P 63
PORTAL COST COST BAXISON CHECK ERON, OX	COMP 64
STATESTON INTERPAL NO. 19. 24.	040 65
CC TO MANO THE TAX TO A CONTRACT OF THE CONTRA	OND DE
Cafes On allegan of at come was a	LT GEO
A 10 100	040
	DMP 70
	OND 71
TOTAL	04P 72
NOTE OF STREET	0.4 7.5
100 MCM A 12.1. STATE A 100 MCM	0.57 74
10 (10 d	
Marie Control of the	
FORMAT (10% - 20m) LICAT MINISTER CHES. COORS.	0MP 77
i i	
STATES OF THE PARTY OF THE PART	70
	00 440
GU 10 (245,200).	
CHECK ON NUMBER OF	70 ALC
O WINDA	
(701) 42 B 7742	
Di 210 4 8 1, WIJ	A B GAL
ひという (メーク・アン) かる マ メンシュ	0.5 B 2
JP (2 0 MT) R20, 240	020
- [00 GEU
PURE CHECK GOND TONE CHECK CHECK GROW, 6X,	MAP 46
'AR '61 'UN TRAUBLING ONE STORE THE	10 d=0
ACT 10 CAL BANK DE 13)	~
240	DAP +3
CASE CASE TABLE STREET OF TABLE SEPTEMBER OF TABLE STREET	0.00
MIGHT A	18F 95
O E YEUR	
FL11 0 R12	
00 250 J m 1, m 1, m	
106 250 NCH # H(1(1,1) + MCH	
[F (NIED! - NCHA) 240	100.00
- 1	0xP162
PORTER CHOIL SAN ANDING TRACK CARON BELL	WP163
181 181 181 181 181 181 181 181 181 181	100164
Capter On Albanto Oc. Str.	2014
1	2007 200
5 10 10 10 10 10 10 10 10 10 10 10 10 10	340102
ACHE B O	227 200
110 MIEL A MERICE	40 TAK
1254 - B C 968 00	
NOT O TOTAL DISTRICT OF MENT	
CONTRACTOR OF THE PARTY OF THE	
300 PF176 (0.510) [. MTERT STATE	

System 1 mE	4000	72/70 00/101 17.37.33.	PAGE 3
911	210	FORMAY CLAY, SIMPONICHAANDARD REACT EMERY EMERGE AN. COMPILS	
	-	GHAILBLOW NO. 15, 4X, 7MMT	
		CHECK ON MUMPER OF TOUCH-AND-GO ONE GO PER LIFETINE COMPILE	
ASA	22	97 (01/2) 0 1 (01/2) 0	***************************************
		510 3 0 1 41661 COMPLET	
	2	NETAGE OF THE SECTION AND SECTION AS CONTRACT	
	340	MITTE (6, 550) I. NTEST. WENT	
125	955		
		MCONT B 1	
	9	CHECK IN MITTHER OF LANGING TAXE PAY HUMB PER LIPETINE COMPSES	
41.	2	OF CALOU	
		TITLE BELTCOME	
		5.6 July 1 = 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m	
	2.2	MAINTENED CONTRACTOR STATES AND A CANAL STATES AND	
551	300	THEST (00,500) IN PEST, MONE	
	240	FORMAL TANK AND THE TAX WAXRAUM CITCH EROOM, SAL.	
		ANGOLAN STATE AND ANGOLAN STAT	•
	000	・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・	
140		00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	010	できょうしょう サイド・ファイン サイン・マー・ファー・ファー・ファー・ファー・ファー・ファー・ファー・ファー・ファー・ファ	
		IF (NIEST - NCHA) 420, 440	
3.0	2	PERSONAL PROPERTY OF THE PROPE	
201	1	STATE OF THE PROPERTY OF THE P	
		CHECH ON MOTHER DE ETTENES	
		Notice of the control	
150		OSTATOU ON THE TOTAL OF THE TOT	
	959	TSTAINUS THE PROPERTY OF THE P	
	07.0	A TOTAL TO THE TAXABLE TO THE TAXABL	
	000	FURENA (ACC) ANATATION OF THE PROPERTY OF THE	***************************************
441	-	10MM 38510M MD. 15. SEL PHYLET B. 15. ZEL BHIGHK B. 15) COPO155	
	969	- Avioro	
	200	JF (NCON1) 510, 520	
	913	CALL GUIDE	
	260	DOT STATE OF THE PROPERTY OF T	

05713/74 10.25.17, Page																																																		
377			ر ا				יינ		5	E	2	77		f	1	F	=	-	2	5;	35	7	2	2	₹:	zļ.	9		F	2	=	=	2	:		30	0	ŀ		5	•	-	-					-	2	
5		Ē	ŧ	27	3	;	2	12	ភ	נו	וני		E	2772	7772	2	3	3			F	7	4	2	7	i	Ļ	1	F	1	7		زو	Ł	1	10	2	ا	يا	2	اد	2	ار	ب د د	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	راو	2	را	23	
BURNOUTINE CALC 74774 GPTEL	SUBROUTER	SUBSTRICT TO SECUENCY FILE FOR SECUENT STORY SECTIONY SECTIONS AND	TANGET TANGET OF THE PARTY OF T	TENSION BECTA	1. SF4(12,10,20), BF6	BLTH(12,20), TF(12,10,20), STGJ(12,20),	BIRCOL 2001, TEMP(300)	. NFE(12.10.20) WITH (12.20), NFP(12.10.20),	WF(12, 10, 20), WEST(17, 24), DEPLY (12, 20),	4(12), APP(12,10), APK(13,16) BEEFE	(12), HINCISS, HP(12,10), PTGIT(12), HTEF/15	27, NEWP (12), NYP (12), NPP (5:12,18), NLP (12)	LUNY DE LA LAC (3, 12, 10), NUMPL (12)	TOTAL FATTE TOTAL OF MS (20)	TVALENCE (PICAL)	1 (P(715), 8PP), (P(3114), are)	3 (170.5) 8(1) (P(0.5) (170.5) (170.5) (170.5) (170.5) (170.5)	(P(11215), 8761), (P(1151	"[68], ("(12[[5], TEAP]	LYALENCE (N(11), NCABE), (N(12), NH),	AS AND	VALENCE THY AND THE	VALENCE (ACCUST, MYP)	74(3115), NFNJ, 78(5816), DRES), (W(#515), KLTH), (K	130 (N(11515), NTGE),	NJ, (N(11845), NFP),	H (1625), M(I), (N(12220), M	6), (A(12866), HEY	VALENCE (WITSAIRY, MYEY	P), THIT	2 (M. (2020) 1000 (1000) (M. (1000) 1000) 1000 (M. (1000) 1000) (M. (1000)		AD THE PARTY INTEREST	40 0 m / 4 m v		AS THE PLICHT NUMBER EGUAL TO GRE	207 P	は、これのようなできます。 おおかまま かかい ログ・イング アンカー・ファイン アンカー・ファイン アンカー・ファイン・ファイン・ファイン・ファイン・ファイン・ファイン・ファイン・ファイン	0 0	是 /1 = 1,05	SOUR + (I) HHNY = SOUR	26	TO A GROUN A X B TRANSPORT			12 CR (N - 13 CR)	32	112	

	36	NUMBER (17 & REPRESENTED & 1)	EALC 96
99		HITE (6,70) T. NUMMLYS	בארב פֿפּ
	TOTAL	CLOK, LONERROR GIGNAL RO, L. AN, UNI W. IS, AN,	בארכ פס
34	72	1 = 86141 1 - 10108	19 2772 19 2712 201
2		07 TO 170 BELY 108 DETY 108 DE	CALC 62
	11	THESE STATES	0410 64 0410 64
	110	1P (488PT - NUMBPT(880H)) 170, 120, 120	בעונ פפ
24	121	ESCR S TAGES	CALC AT
	9.5	TP (HNUM - MNUMS) 176, 176, 150	69 2772
	251	IF (NEPT - HIGHW) 161, 161, 165	בערכ גו
13	191	1 !	כער כ אזו
	165	SO TO 170	CALC 712
	C PISSION	BREAKBORN AV CODE	24 2172
		TAKE CHE TAXE	CALC 73
	N 8 X	PLTGAT	C41C 75
		LANDING SPERCY	CALC 76
		YOURHOLD SED LANGING	CALC 78
13		MAXIMUM OR TOUCH-ANG-SO LINDING IMPART	CALC 70
	┢	TENERAL CAR	ניונ פו
	BELECT	THE LOAD AND TEMPERATURE BEQUENCE FOR A PLIGHT FOR THIS CAL	S CALC AZ
A		1.8.31	בערב פא
		DEFINE LOAD AND TEMPERATURE FOR AIRCRAFT AT REST	50 272
	ı	A CALLANA	בונ פפ
50		TAKE-OF TAKI LOAD MEDURACE	CALC 66
		1 8 1 90 00	ביונ א
	ι	CALT SEARCE	CALC 42
	1 6, 21, 1MT		CALC 93
		STREES(IL) & STIP(IN)88, INT)	CALC 95
		7EMP(1C) & 1C	בעוב פי
		SECRET A MINIMUM LANG-COFF TEXT LOAD CALL MEMBERS CATABLES AND	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
105			CALC 99
			CALCIO
		173	CALCIOIZ
110	H CN	TOTAL POST TOTAL BEAUTIFUL	CALC 1626
			CALCIOZZ
		CHECK FOR KANGON TINE INTERVALS	71.7.7.52
			74074

#ELCET THE GAMDOM MISSIGN TIME ##FACT THE GAMDOM MISSIGN TIME ## RANG 1

	CONTINUE C CHECK FOR TOCH-AND-GO LANDING SEQUENCE C FOR THE TOUCH-AND-GO LANDING LOAD SEQUENCE	CALCI30 CALCI30 CALCI31
	C SELECT A TOUCH-AND-60 LINEARY THRETT LOAD CALL SEARCE (MTGITTHISS), NTGITTHISS.	EALCI 35 CALCI 34 CALCI 34 CALCI 35
	U, DI, IMT) IL W IL + I 3 TRESSELLS * STGT[MISS,INT]	CALC137 CALC138 CALC139
	126	CALC140
	0 00 INI	CALC145
$\ \cdot\ $	270 TERET LANDING THOSE LOAD	77 (184) (27 (184) (27 (188)
	6. 4. INT	CALCISO
		יורנו <u>ז</u> ן:
	C FORM THE LAMBING TAX! LOAD BEOURNCE	CALC154
	C BELECT A MAXIMUM LANGING TAXT LUBD	47C127
	0, St. 181	יירנוצפ. בארכוצפ
		CALCIÓO
	C GELECT A MINMUM LANDING TAXE LOSD CALL DETAILS OF VICTORIES AND VICTORIES	2912192 Cylc192
	0, 52, 1NT)	CALCIES CALCIES
	מושבת לונות שי מנית ביות מתחים ביות ביות ביות ביות ביות ביות ביות ביות	CALCION
	240 THE TOTAL TOTAL TOTAL TOTAL TOTAL SEGUENCE	4[0169
	APAGE 9 APAGE 4 1	A[C17]
	FORKATC/18X, 46HF[164]-	CACC173
	FORMAT (10X, 15MPLIE	ALC:175
	DISSINGS TONIONE	11017
	FORMAT (9X) 11MLGAG	יורנוגם
	I IIM, DEG NUMBER, 4X, SHSTRESS, 6X, SHTEMP, 9X, IIM, DAD NUMBER,	ALC:81
	П	ALC:03
П	1 101/ BIREBELIOLIS TEMPLISTS 162/ BIREBELISSS, TEMPLISSS	CALCIUS

	71/74 02/61	05/13/74 10.23.17. PAGE 5
04 016	TORALA (120, FIG.0, FIG.6, FIG.6, FIG.6, IZG. FIG.6, FIG.6, CALCION CALCION IF (NUMPL) - MFLY) 350, 360, 360	LOTOTAL
350	AUPT & RUPLY + 1	CALCION
9)	CALC BUIDE	C4LC140
	#ET0%#	בונוזי
235		
	•	

	PANDON LOA COMPUIL YN	FOR LOCATION THE PASSOCIATED WITH THE DO ON TEMPERATURE SELECTION CLEENS IN WESCAR. CLEENS IN WESCAR. MISCE 8 9. DO AN WESCAR. MISCE 8 9. MISCE 8 9. MISCE 8 9. MISCE 8 40. MISCE		######################################
<u> </u>	SAME SHAME STANDS	N. SELECTION CROP. IN PROCESSION OF THE PROCESSION OF THE PROCESSI		2 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
00 01 01 01 01 01 01 01 01 01 01 01 01 0	C 50 PENUVE SEL		- MC - MCMT 5 47. 944656(1) 0. HKG 0. 15. 97.	2. 1. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.

Avenui Lie Beants 1977a Offes	PTN 4.0:P253 62/01/74	62/01/70 17.37.30. Pigt 1
NAME OF THE PERIOD OF THE PERI	TOTAL	
THE DESCRIPTION AND PARTY OF THE PARTY OF TH	STEPAN APPOCIATED MITH THE BOCH S	
DIPENSION MSEG(12.	201 201	
COMPUTE THE SATEBUAL FOR THE	KANDUR BELEGIION	
DU 10 1 B 12 MCNT	Z ASS	
10 12 12 13 15 15 15 15 15 15 15 15 15 15 15 15 15	A NISEG	
20 VALTE (6.19) NAY.	6- 13-66 3- 13-66	
30 FURMAT CLON. FORNISEG LESS 1	HAN PERO, 4X, SHNKY B. 15.	
MAKE NANDOM SELECTION FACTOR	INTERVAL 1 TO RISEG	
40 X E EA'.F(1)	\$1 HOMB	
C LOCATE SECRET COLORISON TO NICE	CAN TOWN	
C #	\$ KC. H.	
1 4 4 1 0 1 0 5 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	OF TORS	
	20 Sec. 20 Sec	
20	\$PC# 22	
Dene whereas are and a second	ULATION SPCH 23	
ZUSURE CITUZ BAUUSAY SE	AT LANGE OF THE STATE OF THE ST	
70 milit (0,80) 1, Natu(1)	HANCELD NXY, NO. NC. MCMT BACK 20	
BO FURNAL (LOX, 12HENRUS SIGNAL, 6X	X, 511 8, 15, 4X,	
STATE OF TOTAL STATE OF THE STA	KY S. 15. 4X. 4HAB S. 15. 4X. 4X. BOCK PA	
30 90 1.4 8 1	ADS COLOR	
Nen-34		
6NO	14 31 SPCH 31	

AND THE PERSON OF THE PERSON O		

######################################